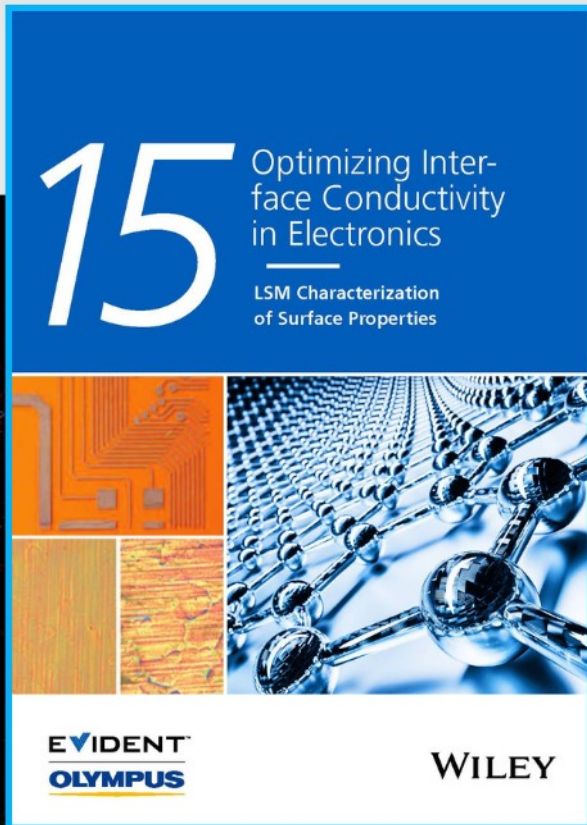




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Ultra-Strong Regenerated Wool Keratin Fibers Regulating via Keratin Conformational Transition

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By virtue of remarkable biocompatibility and their promising applications in biomedical fields, biomass-regenerated fibers, such as wool keratin fiber and cellulose fiber, have attracted extensive attention. However, the insufficient mechanical performance still hinders their yarn manufacturing capability and further large-scale applications. Herein, an ultra-strong and ultra-tough regenerated wool keratin fiber by regulating keratin conformation with high-quality small-size graphene (HQSGr) and mechanical training treatment (M-HQSGr-RWKF) is fabricated. With the assistance of mechanical training, a small addition of HQSGr (0.1 wt.%) remarkably augments the secondary structure transition from α -helix to β -sheet of the keratin, which delivers a tensile strength of 215.4 ± 5.2 MPa, surpassing all reported natural wool and regenerated wool or even poultry fibers. Benefiting from the excellent mechanical strength, wet-state toughness (158.9 MJ m⁻³), and recoverable strain (205.0%), M-HQSGr-RWKF has been demonstrated as a biocompatible artificial muscle to drive the biomimetic motion, which manifests ultrahigh actuation strain greater than 100.0% and stress of 16.7 MPa. The derived ultra-strong and ultra-tough keratin fiber opens a new avenue for developing smart fiber from biomass resources.

1. Introduction

Environmental concerns and strikingly rising oil prices have driven the booming demand on eco-friendly regenerative biomaterials as replacements for million tons of petrochemical products,^[1,2] such as plastics and synthetic fibers.^[3,4] As a representative category of regenerative biomaterials, biopolymeric nanofibrils including cellulose in plants,^[5-7] bacteria,^[8] chitin in crabs,^[9,10] keratins in spider silk,^[11] silkworm silk,^[12,13] wool,^[14] and collagen in mammalian ligaments or other organs,^[15] could serve as universal nano-building blocks for premium regenerated bio-fiber production according to their wide availability, sustainability, and biocompatibility.^[16-19] These biopolymeric nanofibrils usually present analogous structural specialties, reassembling the nanofibrils into sophisticated meso-architecture with controllable

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orientation and crystallinity could result in regenerated keratin fibers with novel engineering material designs and consequent exceptional mechanical properties.^[20–24]

Wool is a noteworthy keratinous fiber, which is the most important animal fiber used in textile applications by far.^[14] More than 2.5 million tons of wool are produced annually worldwide mainly from Australia, China, New Zealand, Iran and Argentina.^[25,26] Simultaneously, a large number of waste wool close to the annual wool production were produced from shearing/weaving trimmings, discarded low grade coarse wool, and fast fashion industry.^[27] However, based on current wool waste treatment industry, such a tremendous number of keratin-rich biomaterials are mainly treated as low-value feed additives, cosmetic ingredients and waste water treatment agents, or even directly end up in landfill or incineration.^[28–30] Recently, producing regenerated fibers from wool keratin (WK) offers a novel and effective high-value strategy for the disposal of waste wool, leading to a significant reduction in carbon footprint, making it a highly sustainable and eco-friendly strategy.^[31–35] Owing to the typical knotting/weaving process and abrasion/stretching requirement for textile products, there is a series of rigorous mechanical requirements for fibers applied in textile industry, such as acceptable tensile strength, sufficient strain-to-failure (above 10%), and elastic modulus between 30 and 60 g per denier (3.4–6.8 GPa).^[36,37] The current limited tensile strength of ≈ 137 MPa is still far from satisfying the mechanical requirement for yarn manufacturing and textile industry.^[34] WK materials exhibit a complex hierarchical structure, across from nanoscale polypeptide chains, intermediate keratin filaments, microscale aggregates, to macroscale compact sheaths, porous cores, and linear threads.^[38,39] Although the complicated hierarchical structure brings great difficulties to reconstruct the biomass fibers, the keratin fibrils could also be an efficient building block for assembling fiber with high mechanical strength.^[40–43] Therefore, engineering the keratin fibril structure remains an attractive strategy to build regenerated wool keratin fiber (RWKF) with high mechanical performance for meeting the industrial manufacturing demand.^[44–47]

By virtue of its atomically thin structure and conspicuous mechanical performance, graphene has widely been used as a reinforcement for bio-composite fibers.^[48–56] However, the underlying reinforcement mechanism, such as the graphene-induced conformation transitions and their effects on fiber mechanical behaviors, has been seldom discussed. Herein, we fabricated an ultra-strong and ultra-tough RWKF by regulating keratin conformation with small addition (0.1 wt.%) of high-quality small size graphene (HQSGr) and mechanical training treatment (M-HQSGr-RWKF). The HQSGr triggers the conformation transition of keratins onto graphene within a distance of ≈ 12.1 nm that is much larger than the thickness of graphene (0.3 nm). Such a wide range of keratin conformation transition from α -helix to β -sheet and thereafter mechanical training induced alignment and densification of these structures remarkably enhance the mechanical performance of RWKF. Benefiting from the ultrahigh strength, wet-state toughness, and recoverable strain, the M-HQSGr-RWKF has been assembled into a fiber-shaped biocompatible artificial muscle with ultrahigh actuation strain (>100.0%) and stress (16.7 MPa), outperforming the state-of-the-art biomaterial derived systems.^[57–60]

2. Results and Discussion

2.1. Continuous Preparation of M-HQSGr-RWKF via Wet-Spinning

Figures 1A and S2C, Supporting Information, schematically illustrate the wet-spinning preparing process and the continuous evolution from keratin fibril dispersion into M-HQSGr-RWKF. First, only small addition of HQSGr (0.1 wt.%) flakes have been uniformly mixed in the WK dispersion while preparing wet-spinning doge. Surfactants such as sodium dodecyl sulfate (SDS) have been added into wet-spinning dispersion to introduce electrostatic repulsive force to assist HQSGr flakes dispersion in alkaline $\text{Na}_2\text{CO}_3/\text{NaHCO}_3$ liquid. Simultaneously, we also optimized the keratin extraction and pure RWKF wet-spinning process to guarantee high-quality matrix fiber for deep reinforcement. As illustrated in **Figure 1A**, directed by fluid-induced shear force, the HQSGr flakes tend to align along the flow direction, especially when the mixed dispersion flows through the narrow spinneret space. In this regard, the aligned HQSGr flakes constructed layered confinement space to intensify the orientation of keratin fibril conformation and even crystallinity transition from α -helix to β -sheet onto graphene within a certain distance. The re-constructing of disulfide bonds during the oxidation bath, combined with the continual stretching of the keratin fibril chains during the mechanical training treatment, finalized in the compact M-HQSGr-RWKF with ultrahigh mechanical performance.

Figure S2B, Supporting Information, depicts the massive production of M-HQSGr-RWKF and pure RWKF with hundreds of meters in length via a consistent continuous wet-spinning technique (yield speed of ≈ 700 m h⁻¹). The scanning electron microscope (SEM) diagrams in **Figure 1B** shows that, after continuous mechanical training treatment, the M-HQSGr-RWKF still exhibits an analogical smooth surface and an approximate diameter of 30 μm compared with the well-definite RWKF. Furthermore, the M-HQSGr-RWKF exhibits remarkable flexibility and high mechanical strength, as evidenced by its ability to be tightly tied into knots. To explore the mechanical properties of pure RWKF, HQSGr-RWKF, and M-HQSGr-RWKF in detail, we resolve the stress-strain curves in **Figure 1C**. In general, all of RWKF, HQSGr-RWKF, and M-HQSGr-RWKF present an elastic deformation at the initial tensile process. After the stress reaches the yield strength, the fiber depicts a conspicuous plastic deformation. The thus-derived M-HQSGr-RWKF manifests a tensile strength of 215.4 ± 5.2 MPa and a strain-to-failure of $8.8 \pm 0.9\%$, surpassing those of HQSGr-RWKF (strength of 181.4 ± 12.6 MPa and strain-to-failure of $10.5 \pm 0.9\%$) and RWKF (strength of 120.8 ± 9.3 MPa and strain-to-failure of $11.3 \pm 1.8\%$) prepared with the same wet-spinning parameters. Furthermore, the other mechanical properties, including Young's modulus, toughness, and weight-bearing ratio (the ratio of the weight that fiber can afford to its own weight) are compared (**Figure 1D**). M-HQSGr-RWKF, HQSGr-RWKF, and RWKF exhibit toughness of 12.9, 10.6, and 9.0 MJ m⁻³, Young's moduli of 6.1, 3.2, and 1.7 GPa, and weight-bearing ratios of 2.0×10^3 , 1.5×10^3 , and 1.0×10^3 , respectively. These results indicate the simultaneous improvement in strength, toughness, and modulus of M-HQSGr-RWKF.

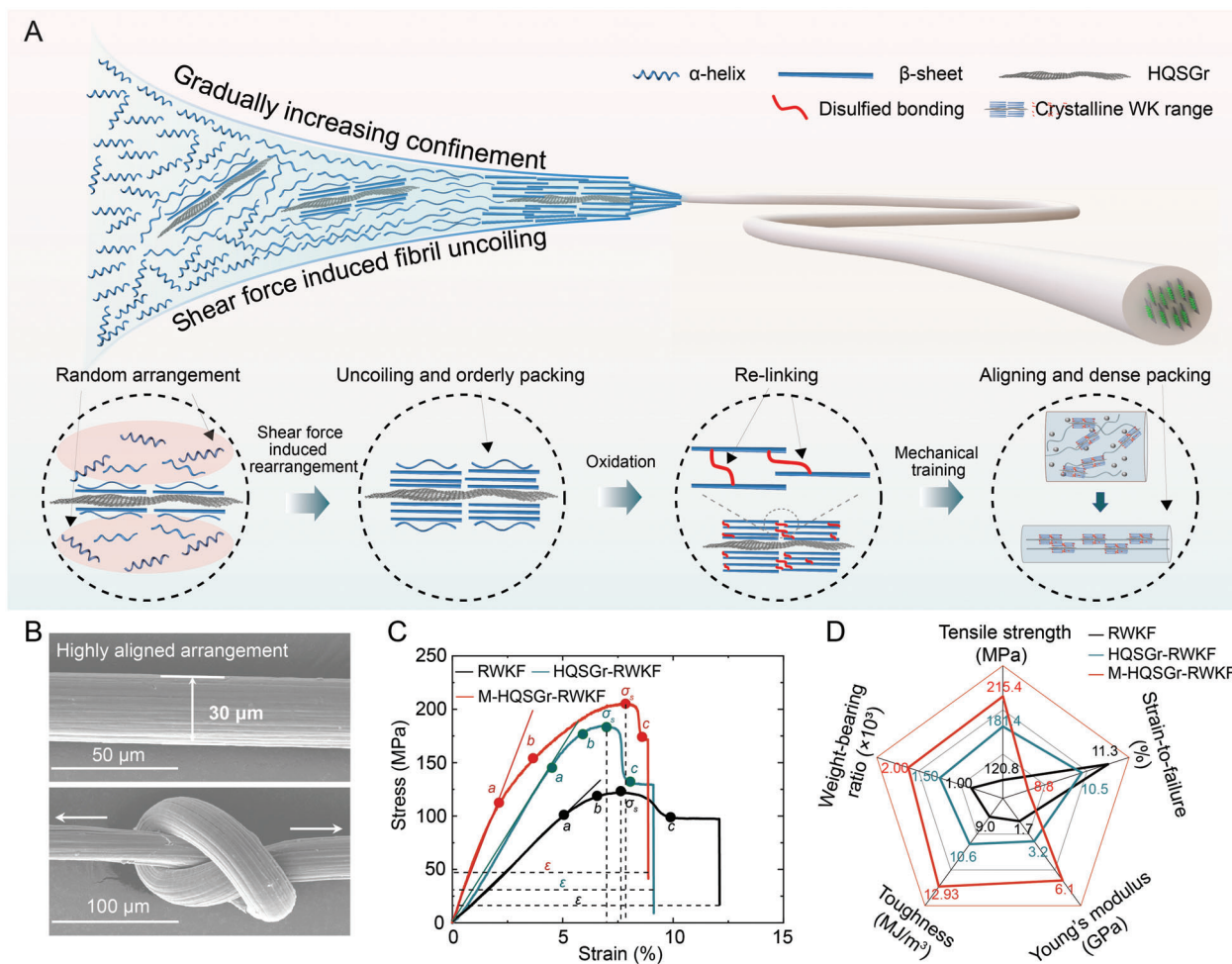


Figure 1. Continuous preparation of M-HQSGr-RWKF. A) Schematic illustration of the M-HQSGr-RWKF wet-spinning process. The magnified graphic highlights the interaction between keratin fibril and HQSGr during the wet-spinning and mechanical training post-treatment. B) Front-surface SEM images of the straight and knotted M-HQSGr-RWKF. C) Stress-strain curves of M-HQSGr-RWKF, HQSGr-RWKF, and RWKF. *oa*: the linear elastic region; *ab*: the nonlinear elastic region; *bc*: the yield region, where ϵ is the strain-to-failure, σ_s is the tensile strength. D) Mechanical performance comparison of M-HQSGr-RWKF, HQSGr-RWKF, and RWKF, including tensile strength, strain-to-failure, Young's modulus, toughness, and weight-bearing ratio.

2.2. Template Effect of HQSGr on Keratin Conformation Transition

The classical theory of composite mechanics is inadequate to explain the substantial enhancement of mechanical performance of M-HQSGr-RWKF via such a small addition of HQSGr (see Text S1, Supporting Information for details). Generally, there are two critical factors to endow the graphene with significant reinforcement effect, i.e., graphene/keratin interaction in wet-spinning dope solution phase and graphene/keratin conformation transition during the wet-spinning process. To elaborate the reinforcement mechanism for optimal design, a series of graphene materials, including small-size graphene oxide (SGO), small-size reduced graphene oxide (SRGO), and large-size graphene (LGr), have been introduced to analyze the effects of surface functionality and size on graphene/keratin interaction (Figures S4, S5, S6, and S7, Supporting Information).

The adsorptions of keratin onto different graphene surfaces were verified from the observation of electron transitions. Amino

acids containing benzene rings (tyrosine, tryptophan, and phenylalanine) undergo electronic transitions when excited by ultraviolet (UV) light and reflected at 280, 275, and 250 nm, respectively. The UV-vis spectra in Figure S8A, Supporting Information, depict evident absorption peak intensity annihilation and blue shift of the peak centered at the specific wavelength of ≈ 245 nm. It corresponds to the strong π - π conjugation between the amino acid and the graphene, which inhibits the electronic transition of the benzene ring. Fluorescence quenching is a powerful technique in the field of researching the dynamic changes of keratin structure in complex systems.^[61–63] The remarkable fluorescence quenching effect in fluorescence spectra further supports the adsorption of keratin onto HQSGr (Figure S8B, Supporting Information). In summary, the HQSGr could serve as an ideal reinforcement phase to build the solid and compact interaction with keratin fibrils.

To provide insight into the structural evolution of keratins, we did atomistic simulations by placing an α -helix on the monolayer graphene. During the structural equilibrium for a

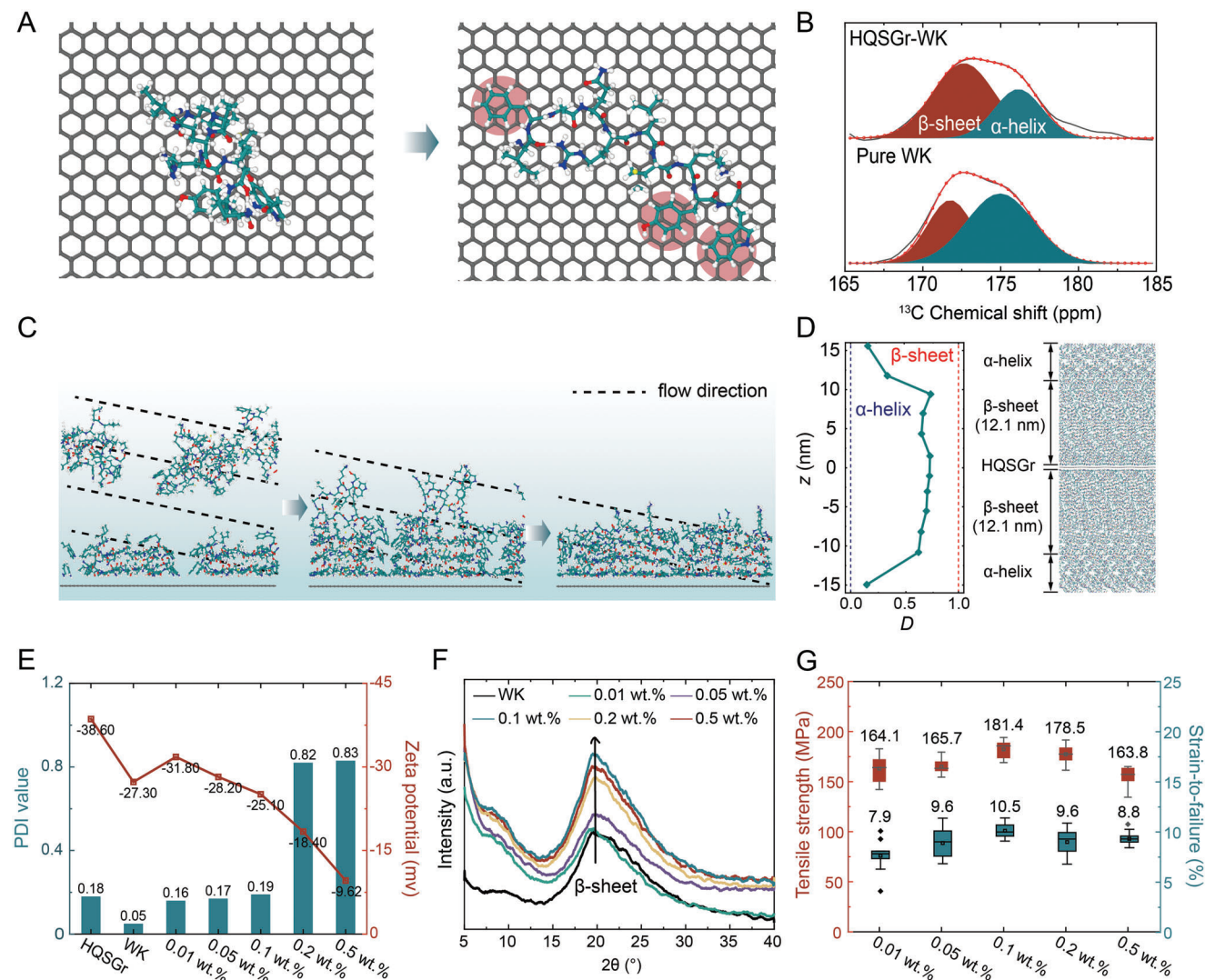


Figure 2. Graphene Surface functionality and size effects on graphene/keratin interaction. A) Structure evolution of α -helix onto graphene before and after the room temperature (300 K) equilibrium. B) Deconvoluted ^{13}C NMR spectra comparison between pure WK and HQSGr-WK hybrid dispersion in a specific range to illustrate the ratio of α -helix and β -sheet. C) Illustration for the flow-assisted ordered arrangement of keratin onto graphene. D) Transition degree and a snapshot of keratins affected by a graphene sheet. E) Zeta potential and PDI values of spinning solutions with different HQSGr ratios. F) XRD pattern of HQSGr-RWKF with different HQSGr ratios. G) Tensile strength and strain-to-failure of HQSGr-RWKF with different HQSGr ratios.

duration of 1 ns, this α -helix spontaneously uncoils into β -sheet (Figure 2A), in which all benzene rings of the keratin closely overlap onto HQSGr because of their strong π - π interactions. This process is also quantified by the increase in radius of gyration (R_g) (Figure S9, Supporting Information). These results indicate that the π - π interaction is crucial to induce the transition from α -helix to β -sheet. The π - π interaction increases the binding stress on α -helix when keratin absorbs onto graphene, which leads to the simultaneous transition from α -helix to β -sheet. Solid-state nuclear magnetic resonance (NMR) spectroscopy has been conducted to characterize the structural information during the uncoiling of α -helix via characteristic chemical shift peak and its offset. As shown in Figure S10, Supporting Information, the comparison of ^{13}C solid-state NMR spectra revealed that the typical peak centered at 54 ppm is ascribed to β -sheet (or random coil).^[64–68] In

addition, the carbonyl resonance located at 173 ppm could be deconvoluted into contribution from α -helix and β -sheet, in which β -sheet ratio (herein, the total content of α -helix and β -sheet is defined as 100%) transmits from 37.8% for RWKF to 66.4% for HQSGr-RWKF (Figure 2B), respectively. The significant peak intensity enhancement at 54 ppm and 175 ppm further supports the prominent keratin conformation transition from α -helix to β -sheet after mixing HQSGr flakes in keratin dispersion, which provides experimental evidence to support our simulation findings.

The wet-spinning fluid hydrodynamic shear stress and drafting confinement are the decisive factors to determine the crystallinity and fibril orientation of the resultant fiber. HQSGr flakes tend to form into aligned arrangement while the mixed spinning fluid extruded through the narrow spinneret. Meanwhile,

the adjacent HQSGr flakes could build a confined space to generate shear force to induce specific range of α -helix keratin fibril close to graphene flakes transmit into β -sheet crystalline stacking structure.

To further understand the enhanced mechanical performance of HQSGr-RWKF, we did atomistic simulations and relevant analyses (see Texts S1 and S2, Supporting Information for details). Based on the classical rule of composite material, Young's modulus of HQSGr-RWKF was predicted as 2.3 GPa, which is much lower than the experimental measurements (3.2 GPa). This is because the classical theory only considers the enhancement effect from intrinsic modulus of graphene (see Text S1, Supporting Information for details). In fact, keratins in the HQSGr-RWKF can be divided into amorphous, α -helix and β -sheet regions,^[15] and Figure 2A demonstrated that graphene can act as nucleating agents for β -sheet crystallization. Considering the enhancement effect from this graphene-induced β -sheet crystallization, we here propose a modified rule-of-mixture to account for the modulus enhancement, which predicts that the range of β -sheets onto graphene is as high as 9.8 nm (see Text S1, Supporting Information for details) from the experimentally measured modulus. To support this prediction, atomistic simulations were performed to explore the nucleation and growth of β -sheets onto graphene. The simulation of Figure 2A shows the transition from α -helix to β -sheet onto graphene, which indicates the nucleation of β -sheets onto graphene. Moreover, the strategy of flow-directed assembly was adopted during the experiment (Figure 2C). The wet-spinning fluid hydrodynamic shear stress and drafting confinement are the decisive factors to determine the crystallinity and fibril orientation of the resultant fiber. HQSGr flakes tend to form into aligned arrangement while the mixed spinning fluid was extruded through the narrow spinneret. Hence, it can be expected that the flow can accelerate the nucleation and growth of β -sheets onto graphene. We further investigated whether the predicted wide range (9.8 nm) of β -sheet crystallization onto graphene sheet is energetically favorable. Herein, a range (≈ 17.0 nm) of α -helices were initially placed onto monolayer graphene, and the α -helices close to the graphene sheet were then progressively translated into β -sheets (Figure S12A, Supporting Information). By fully equilibrating these structures, we calculated the potential energy per atom (ΔE) for different ranges of β -sheets onto graphene with respect to that for full α -helices onto graphene. Figure S12B, Supporting Information demonstrates that ΔE first decreases to negative values and then increases to positive values as the range of β -sheets increases. The negative values of ΔE indicate that the transition from α -helices to β -sheets onto graphene at a range up to 12.1 nm is energetically favorable, which generally supports the above-predicted range (9.8 nm) of β -sheet crystallization onto graphene. To further quantify the structural stabilities, the degree of transition (D) was defined as

$$D = (l - l_{\alpha}) / (l_{\beta} - l_{\alpha}) \quad (1)$$

where l and l_{α} represent the end-to-end lengths of keratin and fully equilibrated α -helix, respectively, and $l_{\beta} - l_{\alpha}$ is the difference between the lengths of fully uncoiled β -sheet and fully equilibrated α -helix. Upon equilibration at room temperature (300 K), the result indicates that such a wide range of β -sheet crys-

tallization onto graphene can maintain the structural integrity (Figure 2D). To summarize, β -sheets can nucleate and grow onto graphene because of the strong bio-nano interfacial interactions, and the growth of β -sheets onto graphene therein can be accelerated by the flow-directed assembly. Once the assembly is completed, a wide range of β -sheets onto graphene is energetically favorable and the integrity of this structure can be maintained. Therefore, the enhanced modulus of HQSGr-RWKF is attributed to the reinforcement of graphene and β -sheet crystallization onto graphene.

Afterwards, we systematically optimize the addition of HQSGr and investigate its effect on the dispersibility and reinforcement (Figures 2E and S13, Supporting Information). HQSGr with a series of ratios, such as 0.01 wt.%, 0.05 wt.%, 0.1 wt.%, 0.2 wt.%, and 0.5 wt.%, have been mixed in the keratin wet-spinning dispersion to evaluate its dispersibility and reinforcement effect on keratin crystallinity, fibril orientation, and fiber mechanical performance. The sedimentation experiment and Zeta potential characterization have been first utilized to evaluate the dispersibility of the mixed dispersion. After 12 h sedimentation, the HQSGr and WK mixtures (0.01 wt.%, 0.05 wt.%, 0.1 wt.%) present consistent stability. Figures 2E and S13, Supporting Information demonstrate that 0.1 wt.% HQSGr mixed WK dispersion exhibits a Zeta potential of -25.10 mV and polydispersity index (PDI) of 0.19, which achieves the maximum graphene content while maintaining the mixture stability. Afterwards, polarizing microscopy has been conducted to monitor the keratin fibril aggregate structure after introducing HQSGr flakes with different ratios. As shown in Figure S14, Supporting Information, the distinct anisotropic birefringence for wet-spinning 0.1 wt.% HQSGr-RWKF indicates its conspicuous keratin fibril orientation. In comparison, 0.5 wt.% HQSGr-RWKF tends to form into stacking flakes at the beginning of wet-spinning, resulting in the edge-only keratin alignment. Figure 2F depicts the X-ray diffraction (XRD) pattern for HQSGr-RWKF with different hybrid HQSGr ratios. 0.1 wt.% HQSGr-RWKF presents the most prominent diffraction peak and the narrowest half peak width located at 19.50° , which corresponds to the crystalline feature of β -sheet. Figures 2G and S15, Supporting Information, summarize the stress-strain curves and mechanical performance of HQSGr-RWKF with different HQSGr ratios, in which 0.1 wt.% HQSGr-RWKF exhibits the highest tensile strength of 181.4 ± 12.6 MPa with the strain-to-failure of $10.5 \pm 0.9\%$. In addition, the high quality of the graphene within RWKF guarantees a tiny amount of defects and impurities. Considering the toxicity of graphene mainly derived from the impurities, only 0.1 wt.% graphene introduction could seldomly lead to safety issues. Graphene in hybrid fiber mainly distributes in the surrounding of wool keratin fibrils. We believe that the use of the HQSGr in fiber production has significant potential for enhancing fiber properties without posing underlying health and safety risks.

2.3. Mechanical Training Post-Treatment

Mechanical "muscle" training treatment has been confirmed as an efficient strategy to achieve the tensile strength enhancement.^[69–71] With mimicking the self-growing mechanism of muscle training, repetitive polymer chain stretching and

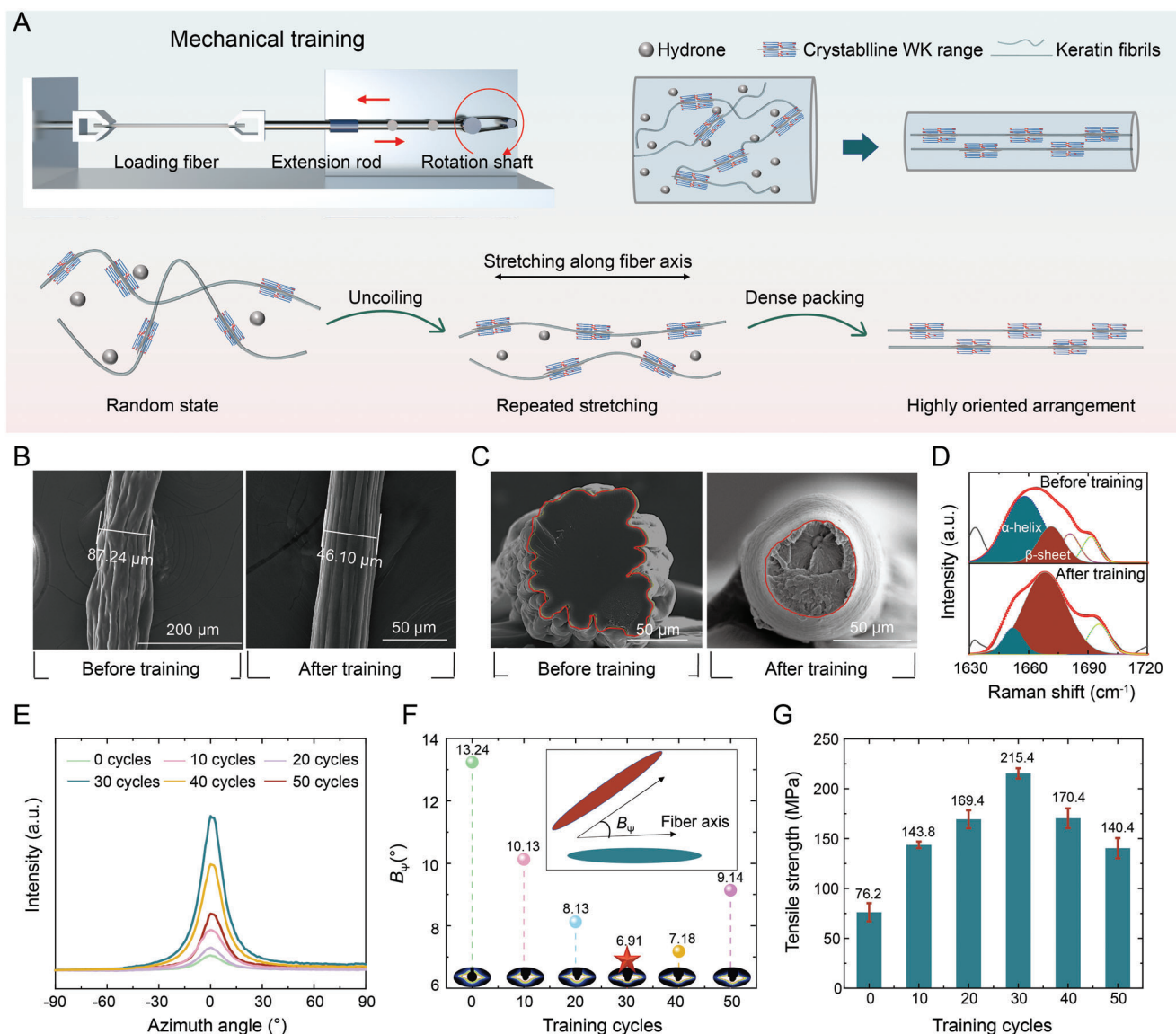


Figure 3. Mechanical training reinforcement mechanism of M-HQSGr-RWKF. A) Schematic diagram of mechanical training mechanism of M-HQSGr-RWKF. B, C) SEM images of the hybrid keratin fiber before and after mechanical training. D) Deconvoluted Raman spectra of HQSGr-RWKF before and after continuous mechanical training. E) The relationship between azimuth angle and intensity under different training cycles. F) Summary of B_{ψ} orientation distribution of the M-HQSGr-RWKF after different training cycles. The inset illustration explains the meaning of B_{ψ} . G) Tensile strength summary of M-HQSGr-RWKF with different training cycles.

effective mechanochemical transduction could construct aligned nanofibrillar architectures with even nanocrystalline domains. These microstructure transitions could significantly enhance the mechanical strength of the trained fiber. As such, the mechanical training post-treatment is implemented to enhance the mechanical strength of the wet-spinning regenerated wool keratin fiber (RWKF) and the hybrid keratin fiber. As demonstrated in Figures 3A and S16, Supporting Information, some randomly coiled keratin fibrils in keratin fibers have been stretched and aligned to demonstrate a short-range ordered feature after continuous repeating slack and drafting on our homemade training facility. The repeated drafting could efficiently facilitate the keratin fibril orientation and the transition from α -helix

to β -sheet. The optical (Figure S17, Supporting Information) and SEM (Figure 3B,C, and S18, Supporting Information) images demonstrate that rough and loose-packing hybrid keratin fiber gradually turns into a smooth and compact configuration, which confirms that the randomly distributed nanofibrils gradually reorient and align toward the stretching direction. Subsequently, upon relaxation of the stretching, the partially aligned nanofibrils will elastically revert back to their prior random distribution, thereby creating additional free volume for subsequent stretching of the fibril chains. As the mechanical training cycle increases, plastic deformation accumulates in the fiber, which gradually elongates along the stretching direction. Simultaneously, the rearrangement of the keratin fibrils could

be also validated through the fiber diameter contracted from 87.24 μm to 46.10 μm , while the mechanically trained fiber also presents a more homogeneous cross-sectional fracture pattern. It further reveals that the nanocrystalline domains in keratin fibrils have been reoriented during the stretching treatment. We also supplement the Raman and Fourier-transform infrared spectroscopy (FT-IR) spectra to analyze the structure transition of the fibril itself. As shown in Figure 3D and S19, Supporting Information, amide I band Raman peak could be deconvoluted to distinguish α -helix (1650–1660 cm^{-1}) and β -sheet (1670–1680 cm^{-1}).^[72] As the mechanical training cycle extends, the β -sheet contribution gradually increases from 28% to 79% to reach the maximum tensile strength at 30 cycles training. The FT-IR spectra verified the coincident phenomenon of the crystalline domain variation tendency (Figure S20, Supporting Information).

To optimize the mechanical training impact on the mechanical properties of hybrid keratin fiber, we systematically increase the training cycle from 10 to 50 cycles to investigate the evolution of microstructure. Meanwhile, we increase the preset draft ratio (λ) from 1.6 to 2.4 to match the fiber length extension. The keratin fibril alignment reaches a steady state after the training cycle reaches 30. Small angle X-ray scattering (SAXS) has been utilized to semi-quantitatively characterize the fiber orientation (Figure 3E,F). The features (such as shape, size, distribution, and orientation) of the particles (including voids) can be studied by analyzing the SAXS patterns.^[73–75] First, the relationship between scattering intensity I and azimuth θ was further analyzed via Fit2D (Figure 3E). As the training cycle increases, the peaks along the prestretched direction become more pronounced, indicating the remarkable improvement in the orientation of keratin fibrils. The diffraction vector q and the reciprocal space vector s can be further obtained via adjusting parameters about Fit2D. Herein, the relationship among parameters is as

$$s = q/2\pi \quad (2)$$

More fundamentally, B_{obs} can be obtained by integrating.^[76] B_{obs} is the full width at the half maximum of the azimuthal profile from the equatorial streak, which is related to the orientation and the size of the particles.^[77] B_{obs} is defined by

$$B_{\text{obs}} = \frac{\int I(s, \varphi) d\varphi}{\int I\left(s, \frac{\pi}{2}\right)} \quad (3)$$

Calculate sB_{obs} ,^[75] and then use Origin to conduct linear fit over sB_{obs} . An approximate slope and an intercept can be endowed on this basis. If Gaussian distribution can be used to approximate the orientation distribution of the scatterers, the relationship can be presented as follows

$$sB_{\text{obs}}(s) = sB_{\psi} + \frac{1}{L} \quad (4)$$

where B_{ψ} is the misorientation angle, which reflects the orientation distribution, and L represents the mean length of the scatterers.^[78,79] Through the above calculation method, we obtained B_{ψ} of the fibrils in the M-HQSGR-RWKF (Figure 3F), which reaches the lowest value of $\approx 6.91^{\circ}$ with 30 training cycles. The tensile strength of the M-HQSGR-RWKF reaches the highest

value of $\approx 215.4 \pm 5.2$ MPa with 30 training cycles (Figure 3G), which is consistent with the azimuth variation trend. Simultaneous fiber strength surpasses all reported natural wool and regenerated wool or even poultry fibers (see Table S1, Supporting Information for details). Therefore, mechanical training post-treatment has been verified as an appropriate strategy to reach a new record tensile strength with nanocrystalline and orientation optimization.

2.4. M-HQSGR-RWKF Artificial Muscle and its Actuating Mechanism

With the efficient capability to complete movements in response to external stimuli, biocompatible actuators have attracted extensive attention in fields of artificial muscle,^[80,81] drug delivery,^[82] biosensing,^[83] and implantable devices.^[84] The dynamic switch between the uncoiling of α -helix and the recoiling of metastable β -sheet upon uniaxial strain and humidity regulation endow wool keratin as the effective material to offer the programmable stimuli-responsive actuation capability.^[85] As schematically illustrated in Figure 4A, WK could serve as the ideal component to assemble biocompatible artificial muscle according to the similar hierarchical filament configuration and the reversible humidity-responsive actuation behavior.^[15,57] To provide insight on the structural evolution of keratins, atomistic simulations and relevant analyses have been conducted to reappear the transition between α -helix and metastable β -sheet under strain and moisture environment (Figure 4B, Movie S1 and S2, Supporting Information). The simulation snapshots demonstrate the transition from α -helix to β -sheet under tension, and this process was divided into three stages based on the evolution of relative potential energy of keratin (Figure 4C): I) The hydrogen bonds were broken with the increasing energy. II) The angles between adjacent amino acids were expanded. III) The transition from α -helix to β -sheet was completed, and the loading capacity was conspicuously improved at the meantime. On the other hand, Figure S21, Supporting Information demonstrates the rapid transition from β -sheet to α -helix in water via the evolution of transition degree while β -sheet contacts moisture. These results provide the fundamental picture for transition between α -helix and β -sheet, which account for the actuation of M-HQSGR-RWKF observed in experiments. With anisotropic and oriented keratin fibril assembly architecture, M-HQSGR-RWKF is expected to present remarkable actuation performance with transmitting the structural transition on all spatial scales.

Tensile tests for both RWKF and M-HQSGR-RWKF in a wet state (Figure 4D) were carried out to compare the structural evolution in the configuration stretching and mechanical property transforming process. The reversibility further validates the reversible transition from α -helix to β -sheet. The RWKF and M-HQSGR-RWKF show an initial elastic behavior up to the strain of 18% and 10%, respectively (1.7 GPa and 3.2 GPa for Young's moduli of RWKF and M-HQSGR-RWKF, respectively). This corresponds to the reversible α -helix uncoiling process (black line at the initial range). As the strain increases, the α -helix starts to uncoil due to the elongation of irreversible keratin peptide chains (red line range), which causes the taut chain structure to temporarily relax (the temporary decrease of stress). With the

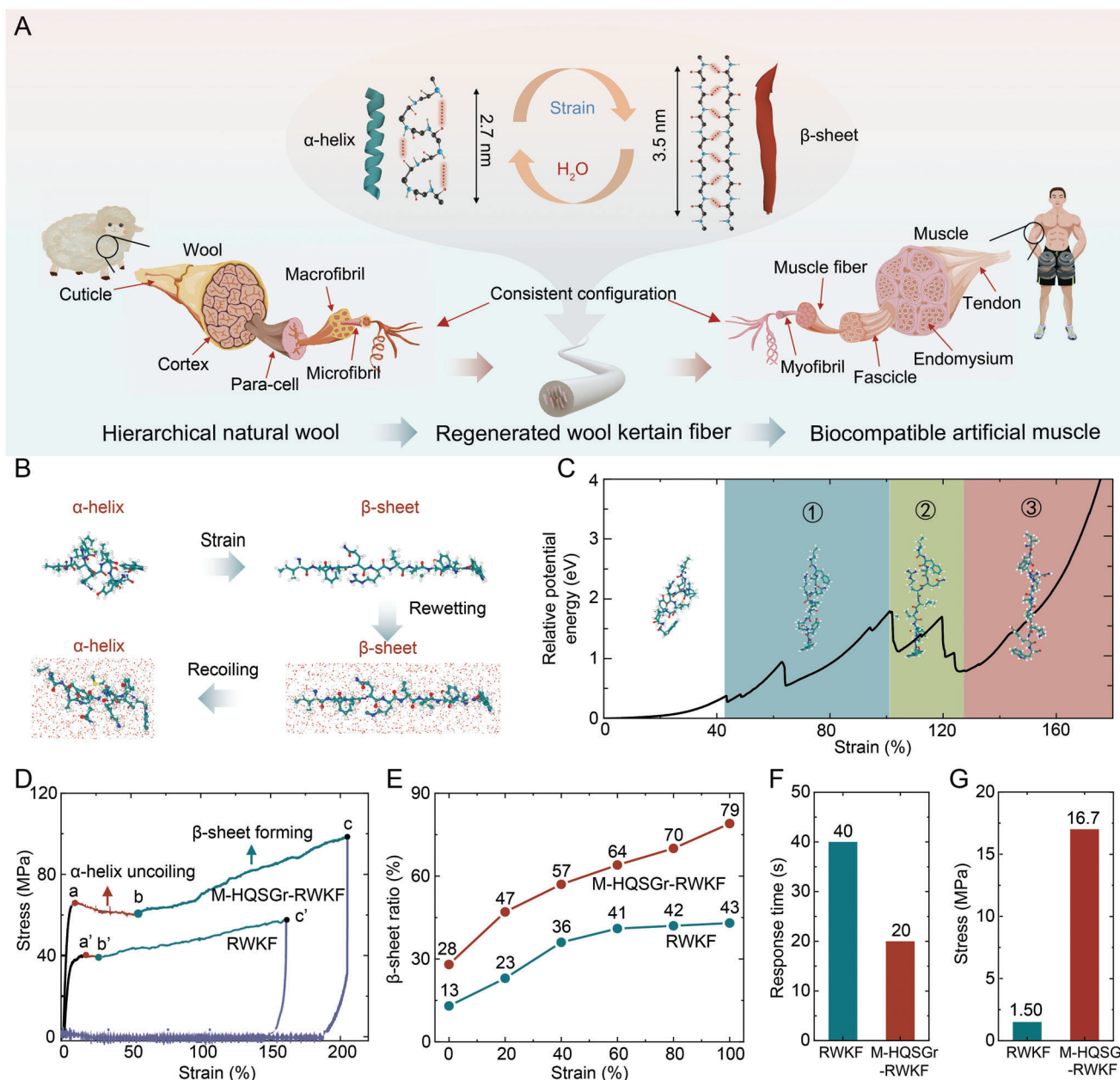


Figure 4. Actuating mechanism of keratin-based fibers. A) Schematic diagram to illustrate the mimicking hierarchical structure from RWKF into biological muscles to produce artificial muscles. B) Atomistic simulation snapshot of the actuation mechanism. The images were collected from Movies S1 and S2, Supporting Information. C) Relative potential energy evolution of keratin from α -helix to β -sheet during the stretching process. D) Stress-strain curves of RWKF and M-HQSGr-RWKF in a wet state. Stress relaxation (ab , $a'b'$ segment) and strain hardening (bc , $b'c'$ segment) ranges are obviously indicated in the curve. E) β -sheet ratio summary for both RWKF and M-HQSGr-RWKF with different strains. F,G) Response time and output stress of both RWKF and M-HQSGr-RWKF.

continuous stretching and the dissipation of moisture, the uncoiled and elongated keratin fibrils maintain stability in their stretched geometry due to the transition from α -helices to β -sheets. The keratin fibrils in RWKF tend to stretch into β -sheets at $\approx 26\%$ strain, corresponding to the strain hardening stage with increasing stress. In contrast, with the addition of HQSGr, M-HQSGr-RWKF manifests a significantly improved stress of 65.2 MPa and an extended α -helix uncoiling process, resulting

in the initiation of β -sheet at $\approx 55\%$ strain and an ultrahigh recoverable strain even beyond $\approx 200\%$. In this region, the applied stress gradually dissipated via the uncoiling of α -helices and the stretching of β -sheets. The long elastic strain of the M-HQSGr-RWKF is in good agreement with the transition from α -helices to the generated metastable β -sheets. For the recovery process of β -sheets back to α -helices, the inducing extra energy is important to serve as the indispensable entropy power to drive the

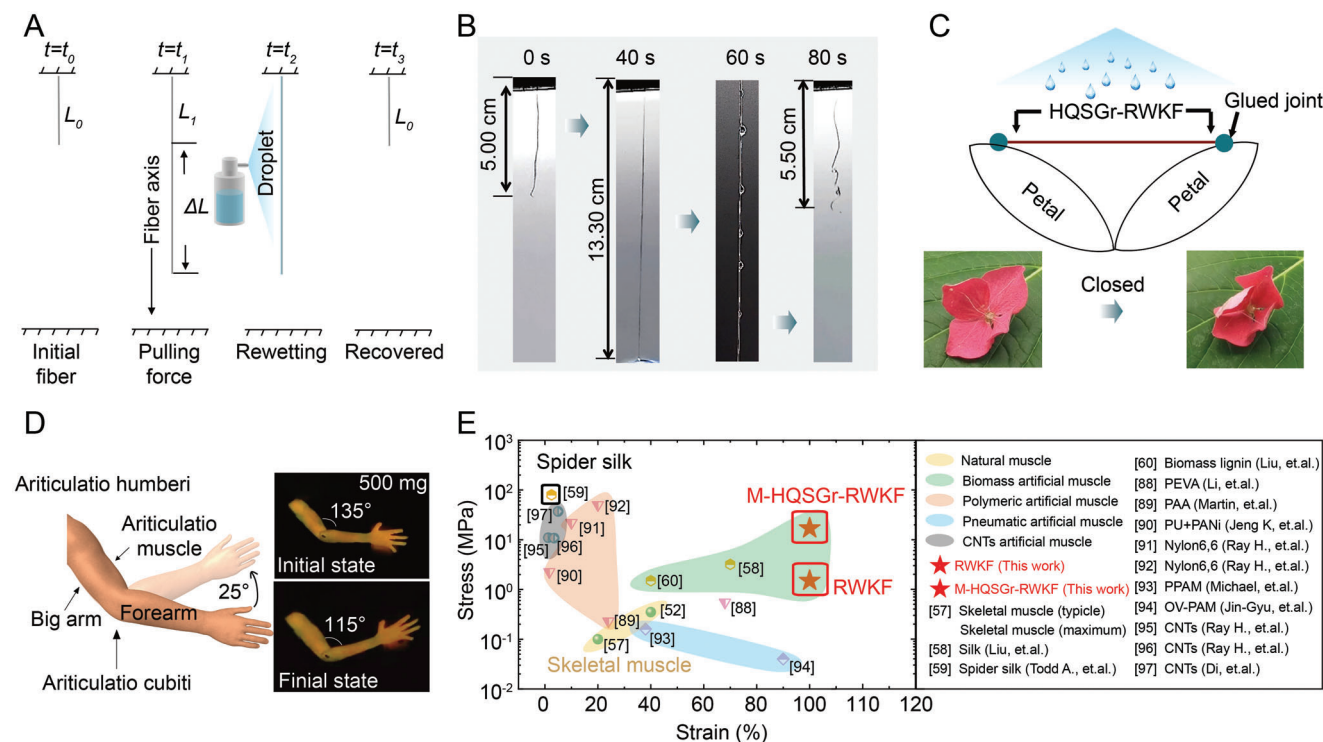


Figure 5. Multi-scene applications of M-HQSGr-RWKF artificial muscle. A) Schematic diagram for the actuation process of M-HQSGr-RWKF. The whole process is divided into four stages, which are recorded at t_0 , t_1 , t_2 , and t_3 , respectively. B) Digital photos of fibers from stretch to recovery. The initial fiber length is 5.00 cm, and the maximum fiber length after stretching is 13.50 cm. The M-HQSGr-RWKF could recover to 5.50 cm, with a strain of up to 140%. C) Automatical close of petals under humidity stimulation driven by M-HQSGr-RWKF. The schematic diagrams illustrate the loading form of M-HQSGr-RWKF on petals, and the whole process could be observed detailedly in Movie S3, Supporting Information. D) Schematic demonstration and optical images of forearm motion driven by M-HQSGr-RWKF artificial muscle, which could be observed detailedly in Movie S4, Supporting Information. E) Output stress and strain comparison between our M-HQSGr-RWKF artificial muscle and reported works. The details could be found in Table S3, Supporting Information.

α -helices formation. While keratin fiber is rewetting, the water molecules re-enter into the keratin interchain and form hydrogen bonds, which prompts the rapid transition from metastable β -sheets back to more disordered α -helices due to the principle of increase of entropy.

Afterwards, we quantitatively characterize the rearrangement of keratin fibril secondary structure by tracking the peak evaluation of the amide I Raman signal, which is deconvolved to α -helix and β -sheet in a separated specific peak range (see Table S2, Supporting Information for details). We monitor the fibril structure variation of both RWKF and M-HQSGr-RWKF via sub-dividing the tensile process into six states with stretching strains of 0%, 20%, 40%, 60%, 80%, and 100%. The local Raman spectral deconvolution for both two fibers at different stretching stages demonstrates that the β -sheet ratio gradually increases upon the continuous stretching (Figures S22 and S23, Supporting Information). As summarized in Figure 4E, M-HQSGr-RWKF presents a prominent increase from 28% to 79%, while RWKF exhibits an augment from 13% to 43%. The conspicuous transition of the keratin secondary structure indicates the possible strengthened actuation behavior. In addition, it has been reported that moisture-induced secondary structure transition can drive the actuation of keratin fiber. For example, Fratzl et al. studied the hydration mechanism of tendon collagen, which provides insights into how water can induce the conformation transition.^[86,87] As

shown in Figure S24C, Supporting Information, RWKF tends to reach moisture adsorption saturation in 50 s with <3.00 mg water adsorption, while M-HQSGr-RWKF manifests over 12.00 mg water adsorption contributed by the consistent fiber mass. We summarized the response time and output stress for both RWKF and M-HQSGr-RWKF in Figure 4F,G. The M-HQSGr-RWKF could achieve an output stress of 16.7 MPa and a response time of 20 s, far surpassing that of 1.5 MPa and 40 s for RWKF. In this regard, M-HQSGr-RWKF is expected to demonstrate fabulous actuation performance.

2.5. Stimuli-Responsive Actuation of M-HQSGr-RWKF Artificial Muscle

The humidity-responsive actuation of M-HQSGr-RWKF artificial muscle has been schematically illustrated in Figure 5A. The initial fiber length is labeled as L_0 . After continuous stretch and dehydration, the fiber length extends to L_1 , accompanied with restoring specific quantities of β -sheets. Afterward, humidity stimulation triggered the fiber to recover its initial length L_0 . The length difference is marked as ΔL , and the output strain is calculated as $\epsilon = \Delta L/L_0$. The actuation capability of these M-HQSGr-RWKF artificial muscles was qualitatively estimated by recording the geometries variation with humidity stimulus when exposed

to water spray at room temperature (Figure 5B), which indicates that M-HQSGr-RWKF artificial muscle manifests a 140% strain within a response time of only 20 s. Meanwhile, the fibrous artificial muscle also presents a high reversibility with gradually improved tensile strength (Figure S24D, Supporting Information). The self-reinforcing phenomenon of M-HQSGr-RWKF artificial muscle also further verifies the strengthening effect on keratin fibers of mechanical training.

After verifying the intrinsic actuation behavior of M-HQSGr-RWKF, we further demonstrate its potential as an artificial muscle with driving flower petal and forearm motion. The stimuli-responsive M-HQSGr-RWKF artificial muscle with reversible stretching/contracting properties can be used as localized “hinges” to control the folding process. After fixing petals along the longitude and latitude directions, the M-HQSGr-RWKF artificial muscle successfully drives the petals under humidity stimulation (Figure 5C, Movie S3, Supporting Information). Otherwise, M-HQSGr-RWKF with only 5 cm length and 5 mg weight have been assembled into an artificial muscle bundle and fixed between the articulation humeri and the articulation cubiti in the polyethylene artificial forearm. The M-HQSGr-RWKF artificial muscle is also demonstrated to replace the biceps to drive arm bending movement, in which the “forearm” is ≈ 8 cm in length and 500 mg in weight (Figure 5D, Movie S4, Supporting Information). After applying extra moisture stimulation onto the fiber, the forearm bent 25° with an output work of 0.04 J in 40 s.

As shown in Figure 5E, compared with other natural muscle (skeletal muscle^[57]), biomass artificial muscle (silk,^[58] spider silk^[59] and biomass lignin^[60]), polymeric artificial muscle (polyethylene vinyl acetate (PEVA),^[88] polyacrylic acid (PAA),^[89] polyurethane-polyaniline (PU-PANI)^[90] and polyhexamethylene adipamide (Nylon6,6)^[91,92]), pneumatic artificial muscle (pleated pneumatic artificial muscles (PPAM),^[93] origami-based vacuum pneumatic artificial muscles (OV-PAM)^[94]) and CNTs-based artificial muscle counterparts,^[95–97] the M-HQSGr-RWKF based system exhibits an ultrahigh actuation strain of 100% while maintaining distinguishing output stress. As a result, with the combination of the systematical analysis for the actuation behavior and demonstration for artificial muscle capability, M-HQSGr-RWKF could provide a bright avenue to customized actuation responsiveness toward broad biocompatible soft robotics or even bionic devices.

3. Conclusion

In summary, we fabricated an ultra-strong and ultra-tough M-HQSGr-RWKF with hundreds of meters in length through a continuous wet-spinning technique. HQSGr has been introduced to regulate the nontrivial secondary structure and polymeric aggregation conformation of keratin, inducing the reinforcement of the hybrid fiber with a tensile strength of 215.4 ± 5.2 MPa, in combination with the mechanical training post-treatment. The ultrahigh strength surpasses all previously reported WK fiber and is even comparable with degummed silk. In addition, M-HQSGr-RWKF has been demonstrated as a humidity-responsive artificial muscle, supported by the water-triggered transition of the keratin secondary structure. The enhanced mechanical strength and moisture adsorption capability remarkably improve the actuation performance to a toughness of 158.9 MJ m^{-3} , an output stress of

16.7 MPa, and a response time of 20 s. Furthermore, inspired by the motions observed in living organisms, M-HQSGr-RWKF artificial muscle has been demonstrated to drive biomimetic motion, such as petal closure and forearm bending. We anticipate that such ultra-strong and ultra-tough M-HQSGr-RWKF could shed light on the development of innovative bio-regenerated fiber manufacturing and stimuli-responsive applications for health-care or personal protection.

4. Experimental Section

Regenerated Wool Keratin Extraction: The process for extracting regenerated wool keratin by reduction method entails several steps, including degreasing, dissolving, precipitation filtration, and freeze-drying.

Degreasing: First, the sheep wool was selected as the raw material of the experiment, and the wool was cut into 1 cm segments. Then, in order to remove the scales of the wool surface, the wool was immersed in 0.1 mmol mL^{-1} sodium carbonate (Greagent, Na_2CO_3 , AR, $\geq 99.8\%$) solution for degreasing, bath ratio is 1:25.

Dissolution: Soak wool in 8 mmol mL^{-1} urea (Greagent, $CO(NH_2)_2$, AR, $> 99\%$) solution, then 10% L-cysteine (Adamas, RG, $> 97\%$) was added to break the disulfide bond. Then 0.02 mmol mL^{-1} sodium dodecyl sulfate (Greagent, SDS, AR, $\geq 90\%$) was added to enhance the dissolution effect. Finally, 1 mmol mL^{-1} sodium hydroxide (Greagent, NaOH, AR, $\geq 96\%$) solution was added to adjust the pH of the mixture to 11, and added the degreased wool with a bath ratio of 1:25. The mixture was mechanically stirred at 363 K for 4 h.

Precipitation and filtration: Filter the mixed solution obtained by dissolving the wool residue to get keratin solution, add 1 mmol mL^{-1} sodium sulfate (Adamas, Na_2SO_4 , ACS, $\geq 99\%$) and hydrochloric acid (Greagent, HCl, AR, 36%–38%) solution to adjust the pH of keratin solution to 4. Then keratin was precipitated and filtered to get keratin solid. Finally, it was washed several times to remove residual urea in keratin.

Freeze-drying: The pure solid keratin was freeze-dried for 48 h to obtain keratin powder. As shown in Figure S3, Supporting Information, the extracted powder is high-quality keratin, which could be served as an ideal source for further RWKF fabrication.

Preparation of Various Graphene Materials: SGO was prepared by oxidation of natural graphite using modified Hummers.^[98,99]

SRGO was prepared by the previously reported methods.^[100] Hydrazine hydrate and ammonia were used as reducing agents and dispersants, respectively. In detail, 100 mL hydrazine hydrate (35 wt.%) and 22 mL ammonia (Greagent, AR, 25%–28 wt.%) were added to 100 mL 0.5 mg mL^{-1} SGO dispersion. Then the mixture was kept at $95^\circ C$ for 1 h to reduce the SRGO flakes.

The fabrication procedures of LGr were conducted according to the literature.^[101] The large graphene oxide was thermally reduced to LGr by high-temperature heat treatment at 1473 K for 30 min.

HQSGr was synthesized according to the previously reported typical methods.^[102] In the microwave environment, methane was used as a carbon source, and SiO_2/Si was discharged in the quartz tube to produce a corona, which was used to directly prepare HQSGr. The resulting graphene can float in the quartz tube-like “snow” for it to collect.

Continuous Wet-Spinning Process of RWKF and HQSGr-RWKF: The key of wet-spinning technique involves the preparation of precursor solution and the regulation of spinning parameters.

For pure WK spinning solution, keratin powder was dissolved in 0.3 mmol mL^{-1} sodium carbonate (Greagent, Na_2CO_3 , AR, $\geq 99.8\%$)/sodium bicarbonate (Greagent, $NaHCO_3$, AR, $\geq 99.5\%$) buffer solution. 10 wt.% DL-1,4-Dithiothreitol (Adamas, DTT, RG, 99%) was added to fully break the disulfide bond in keratin, and 10 wt.% SDS was added to assist in the dissolution of keratin and protect the reduced sulfhydryl group. After stirring for 12 h, the mixture was heated at 363 K for 1 h and placed at room temperature for 24 h.

For HQSGr-WK hybrid spinning solution, HQSGr was dispersed in SDS solution first, the other steps were consistent with the preparation process of spinning solution.

The prepared spinning solution was poured into the reaction kettle of the metering pump, and the reaction kettle was vacuumized for 5 min to remove the microbubbles in the spinning solution. The spinning solution was extruded from the spinneret using a metering pump at a rate of 0.6 cc min⁻¹. Here, the spinneret with an inner diameter of 100 μm and 20 holes was adopted. The drawing ratio of the primary fiber in the coagulation bath is $\lambda = 1$, which means that there is no drafting effect. The drawing ratio of the fiber in the oxidation bath is $\lambda = 1.2$, and the temperature of the dry tunnel is 313 K.

Mechanical Training: A mechanical training device was constructed that uniformly applies a tensile force along the fiber axis, and allows for manual adjustment of the stretch ratio and training rate during the training process. The maximum stretching ratio can reach 2.4, and the maximum training rate can reach 2 cycles s⁻¹. During the training, the fibers were loaded on two fixtures parallel to each other. By adjusting the motor speed, the fibers were trained with 10, 20, 30, 40, and 50 cycles within 60 s. The initial stretch ratio λ was 1.6, and the stretch ratio λ increased by 0.2 for every 10 cycles of training.

Preparation of Fibrous Artificial Muscle: One end of the fiber in the wet state was fixed, and the force along the fiber axial direction was applied to the other end. After 40 s, the fiber was dehydrated and dried. At this time, the length of the stretched fiber could be maintained by removing the force, and the artificial muscle was prepared.

Output Stress Measurement: Own test apparatus for measuring the output force was designed and developed. The Mark-10 dynamometer was sealed to ensure the uniform distribution of humidity in the testing environment. The humidifier was used to regulate the humidity in the confined space, and the fog output was 300 ml h⁻¹. The prepared artificial muscle was affixed onto the jig of the dynamometer, and the position of the jig was adjusted to keep the fiber tight. The resolution of the dynamometer was 5 mN. After the test is started, the output force during fiber contraction was recorded by holding the clamp steady.

Physicochemical Characterizations: X-ray diffraction patterns were obtained from a Bruker D8 advanced diffractometer with Cu-K α radiation (wavelength dimension of 1.5406 Å), and the data were collected from 5° to 40° with a scan rate of 10° min⁻¹. The morphology and structure of the prepared fibers were collected by scanning electron microscopes (FEI Scios) with an accelerating voltage of 10.0 kV. X-ray photoelectron spectroscopy (XPS) was collected through an ESCALAB 250Xi spectrophotometer using a monochromatic Al K α X-ray source (ThermoFisher Scientific). The Fourier-transform infrared spectroscopy (FT-IR) was carried out in an absorption mode (Bruker Tensor 27). The Raman spectroscopy was performed by using a LabRAM HR800 (JobinYvon) instrument with a 785 nm incident radiation and a 50 \times aperture. ¹³C solid-state NMR spectra were collected at 400 MHz on a Bruker Advance III HD 400 WB spectrometer, and the Larmor frequency was 100.6 MHz. WK sample filled in a 3.2 mm diameter ZrO₂ rotor with spinning at 10 kHz frequency. The chemical shifts of ¹³C spectra were reported with reference to tetramethylsilane (TMS) and CH peak from Adamantane. SAXS measurements were performed on a beamline (BL19U2) at Shanghai Synchrotron Radiation Facility. The wavelength dimension of the X-ray was 1.033 Å and the distance between the detector and the sample was 2205 mm. The resulting analysis of the SAXS patterns was performed by Fit2D software.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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Conflict of Interest

The authors declare no conflict of interest.

Data Availability Statement

The data that support the findings of this study are available on request from the corresponding author. The data are not publicly available due to privacy or ethical restrictions.

Keywords

artificial muscles, high-quality small size graphene, mechanical training, regenerated wool keratin fibers, secondary structure transitions

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ADVANCED FUNCTIONAL MATERIALS

Supporting Information

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Ultra-Strong Regenerated Wool Keratin Fibers Regulating via Keratin Conformational Transition

Liang Zhang, Ning Ma, Xiangzheng Jia, Tianjiao Hua, Jin Zhu, Chenbin Ding, Dongzi Yang, Jinrong Luo, Menglei Wang, Jiajun Luo, Shuo Li, Xiaoling Tong, Qiyue Fan, Zhou Xia, Yanyan Shao, Muqiang Jian, Enlai Gao, Yuanlong Shao* and Jin Zhang**

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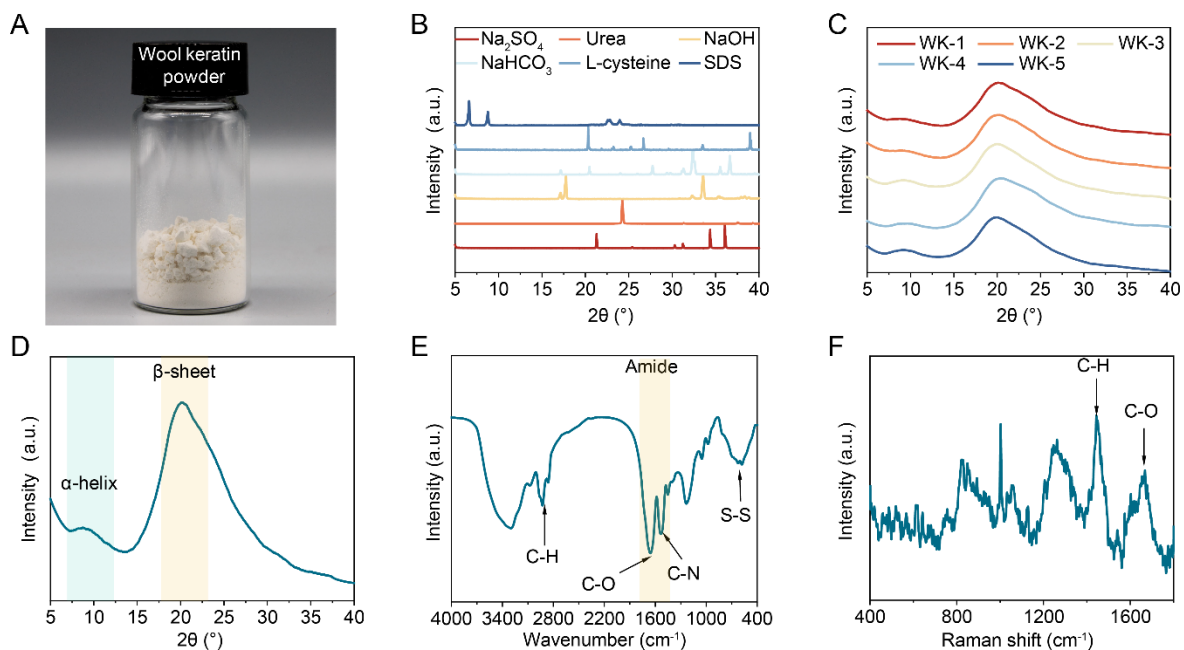


Figure S1. Extraction and characterization of high purity keratin powder. A) Keratin powder extracted from raw wool and waste wool *via* reduction method. B, C) XRD patterns of the chemicals used to extract wool keratin and different batches of extracted wool keratin powder. D) Representative single XRD pattern of wool keratin powder. E) FT-IR spectrum of keratin powder. The characteristic amide bands and disulfide bonds of the protein are clearly shown. F) Raman spectrum of keratin powder.

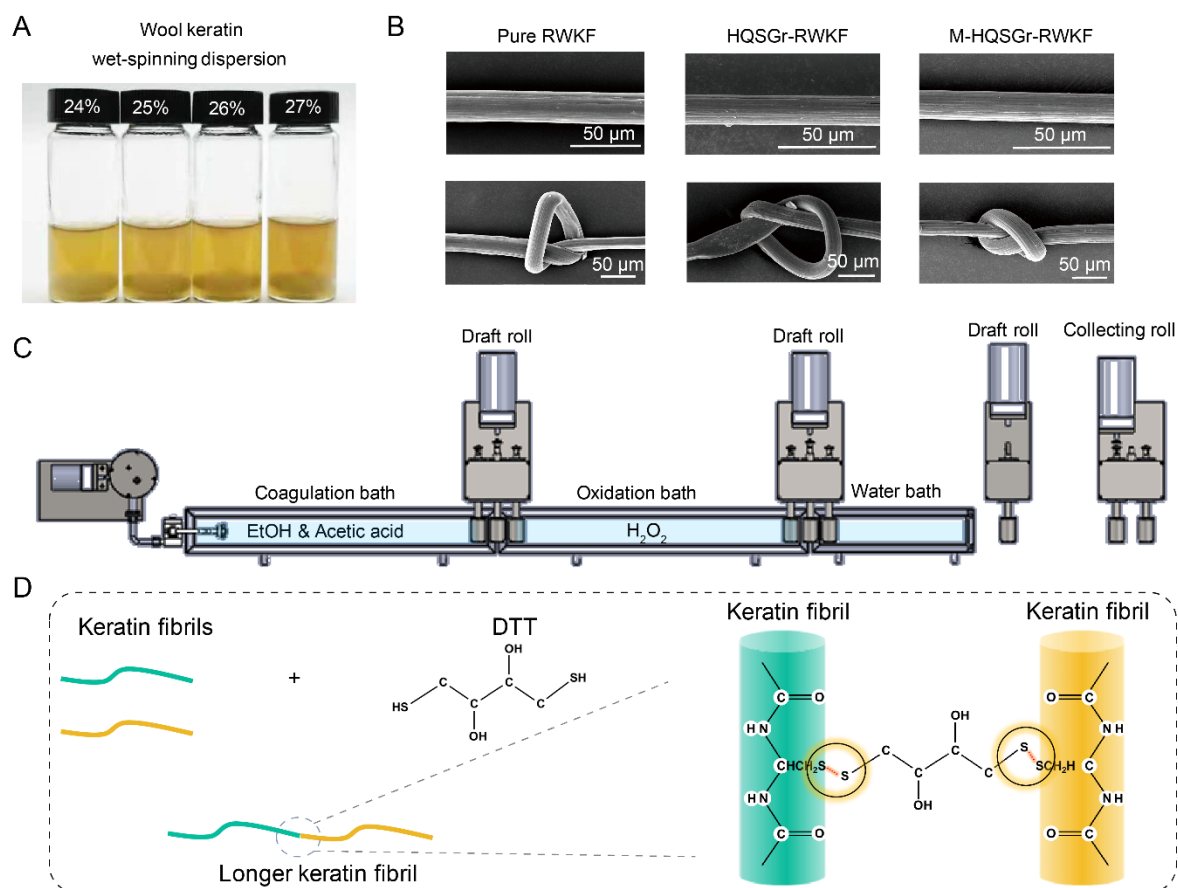


Figure S2. Continuous wet-spinning fabrication of pure wool keratin fibers. A) Wool Keratin wet-spinning dispersion with varied keratin solid content from 24 wt.% to 27 wt.%. B) SEM images of surface and knotting of various fibers. The fiber presents a smooth surface morphology with an analogical diameter of 31 μm . Images of the knots show the difference in toughness. C) Wet-spinning line demonstration for continuous fiber production. D) Schematic diagram of DTT induced keratin chain re-bonding.

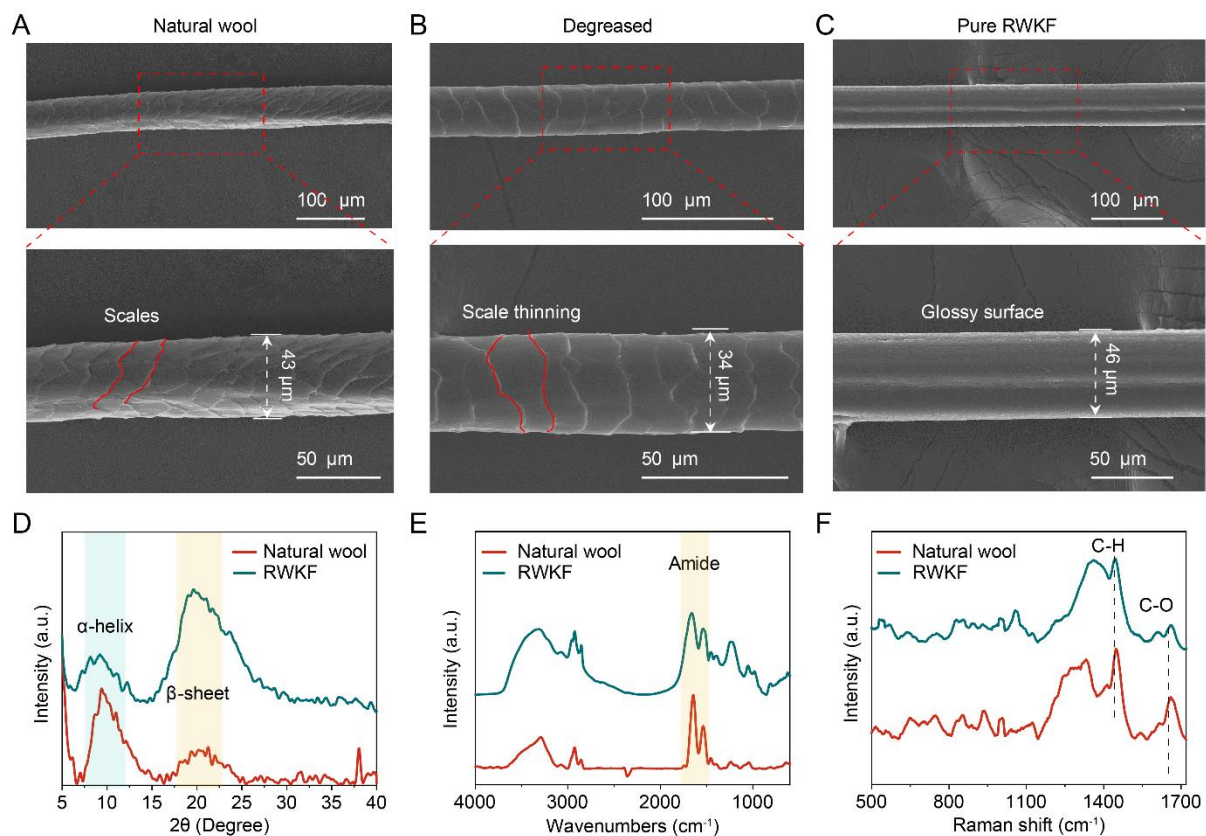


Figure S3. SEM and spectra characterization of pure RWKF. A-C) SEM images of natural wool, degreased wool and pure RWKF (from left to right). D-F) XRD patterns, FT-IR spectra and Raman spectra of natural wool and pure RWKF.

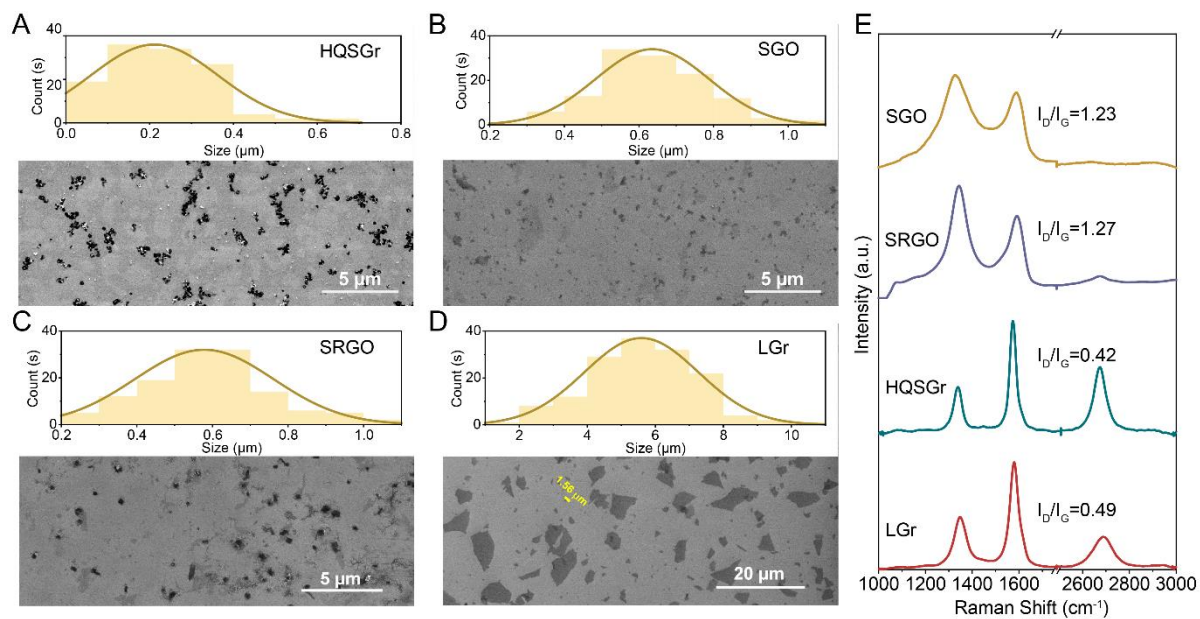


Figure S4. SEM images and Raman spectra of various graphene materials. A-D) SEM images of HQSGr, SGO, SRGO, and LGr captured by SEM, respectively. The inset shows the statistics for the size of various graphene materials. E) Raman spectra of different graphene materials.

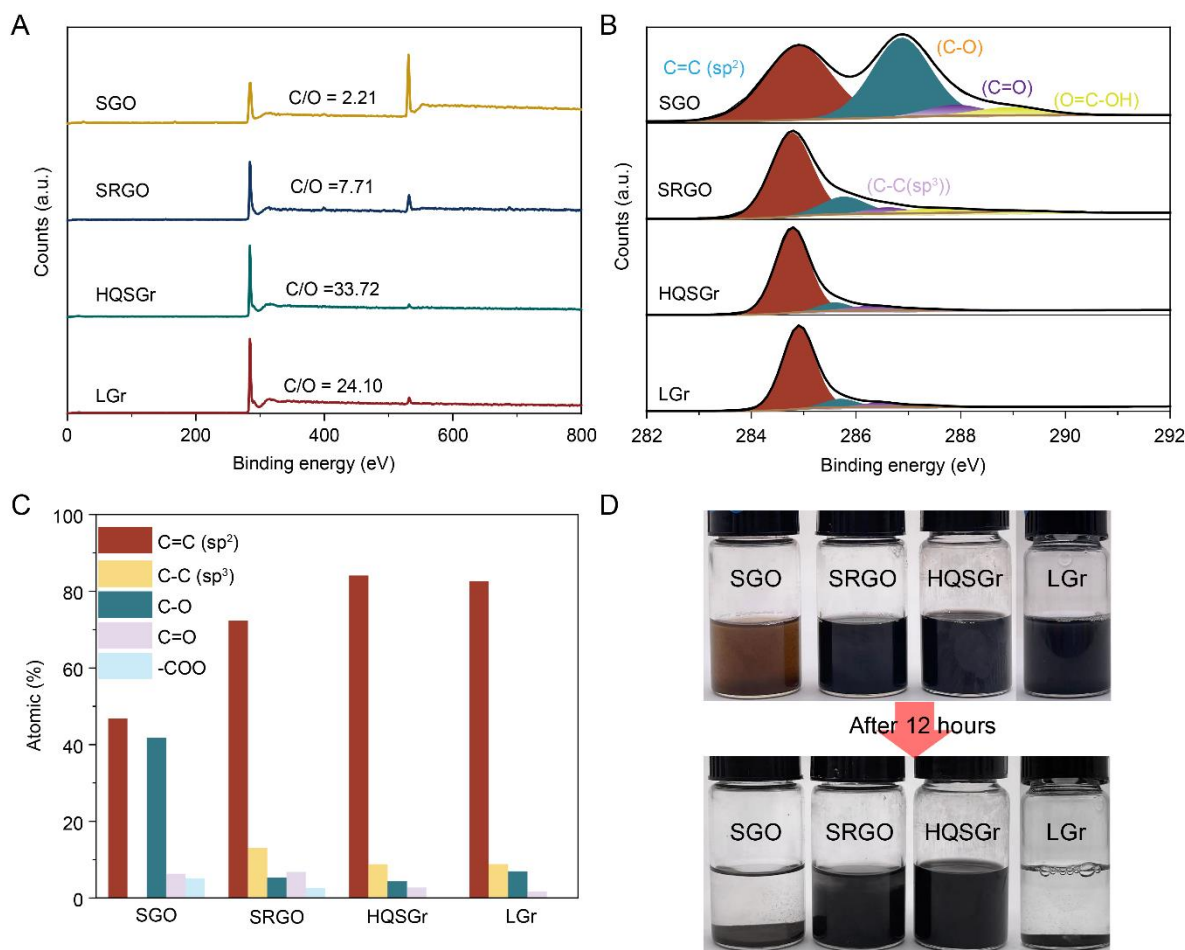


Figure S5. A-C) Chemical composition and oxygen-functionalities of the various graphene quantified by XPS. LGr and HQSGr contain few of structural defects and oxygen-contained functional groups. D) Dispersion and stability of different graphene materials. First, various graphene materials with the same mass (3 mg) were added to 10 ml carbonate buffer, and the dispersion was assisted by adding surfactants and sonicating. After standing for 12 hours, the dispersion results were recorded.

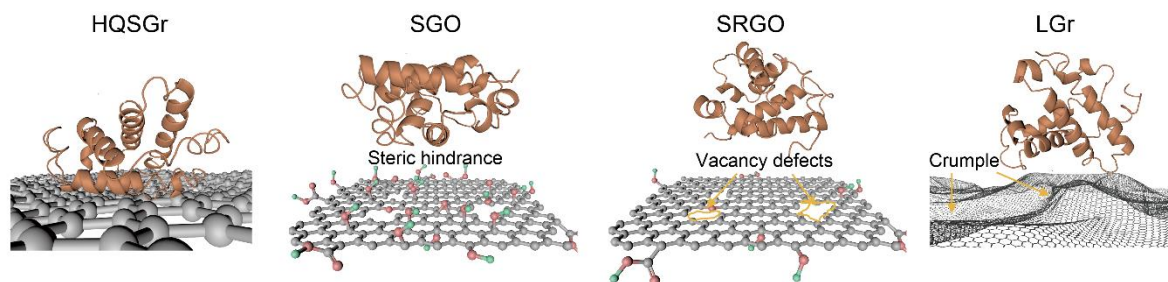


Figure S6. Schematic diagram of interaction between keratin and various graphene materials. The strong face-to-face π - π interaction between six-membered ring on graphene and conjugated aromatic structure on keratin amino acids (such as phenylalanine, tyrosine, *etc.*) will pin the keratin α -helix onto the graphene flake surface,^[1] which could induce the steady attachment of keratin fibril on graphene. However, the oxygen-functional groups on SGO and SRGO sheets could form the sub-nano scale steric hindrance in combination with the vacancy defects to hinder the compact π - π interaction. In addition, the inevitable crumples on LGr sheets also hamper the close graphene/keratin attachment, which subsequently tends to generate aggregation in keratin fibril dispersion.

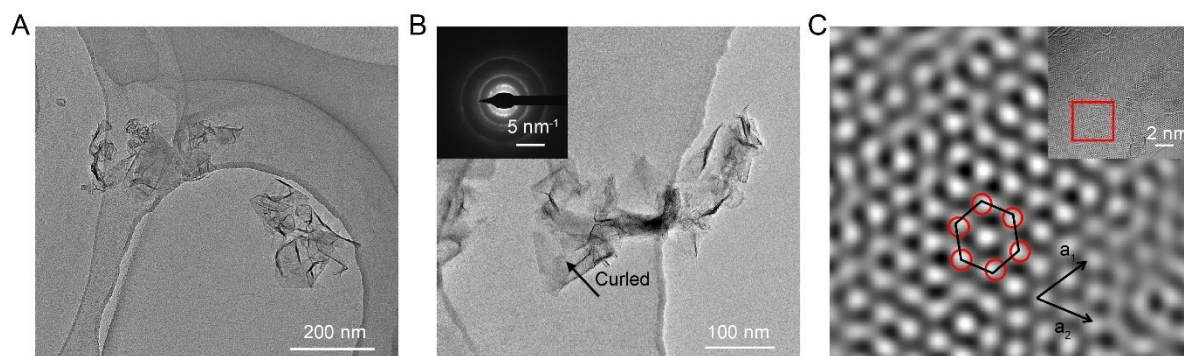


Figure S7. TEM images of HQSGr. A, B) Low-magnification TEM images and selected-area electron diffraction pattern (as an inset) of HQSGr. C) Selected-area electron diffraction pattern exhibiting the sixfold symmetry and low-magnification TEM image (as an inset) of HQSGr. TEM images proved the flake size of ~ 200 nm and the defect-less feature of HQSGr.

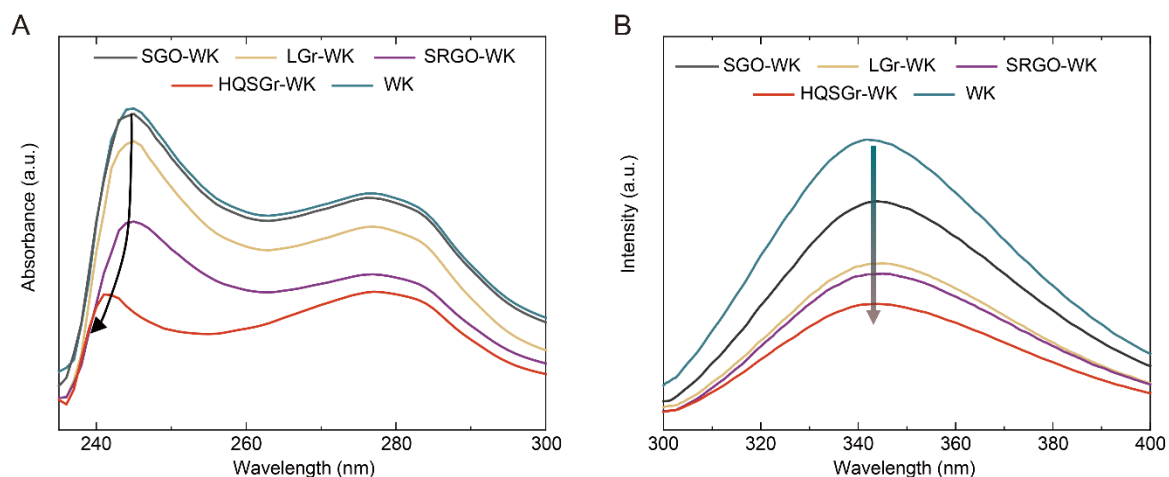


Figure S8. Representation of π - π interaction in spectroscopy. A) UV-vis spectra of various graphene/keratin hybrid dispersions. With the strong graphene/keratin π - π interaction, HQSGr-WK dispersion presents a distinct blue shift from 245 nm to 241 nm, in contrast to SGO-WK hybrid dispersion. B) Fluorescence spectra of various graphene/keratin hybrid dispersions. The fluorescence characteristic peak of aromatic amino acids is located at 343 nm. The HQSGr-WK dispersion presents a prominent fluorescence quenching effect based on that the graphene/keratin π - π interaction suppresses conjugated signal from aromatic amino acids.

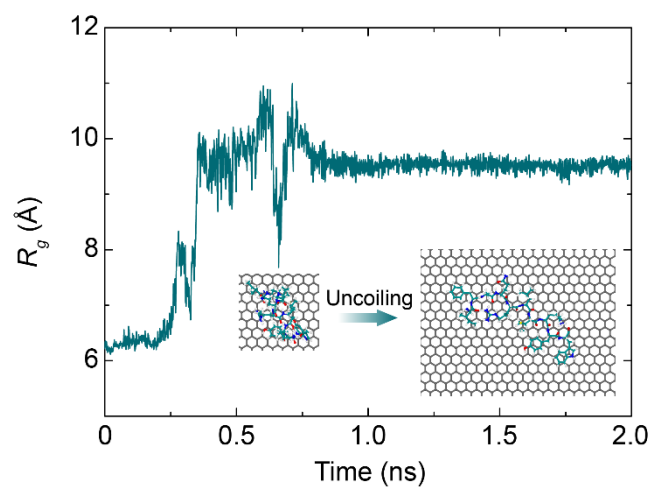


Figure S9. Evolution of the radius of gyration (R_g) of α -helix onto graphene during the room temperature (300 K) equilibrium.

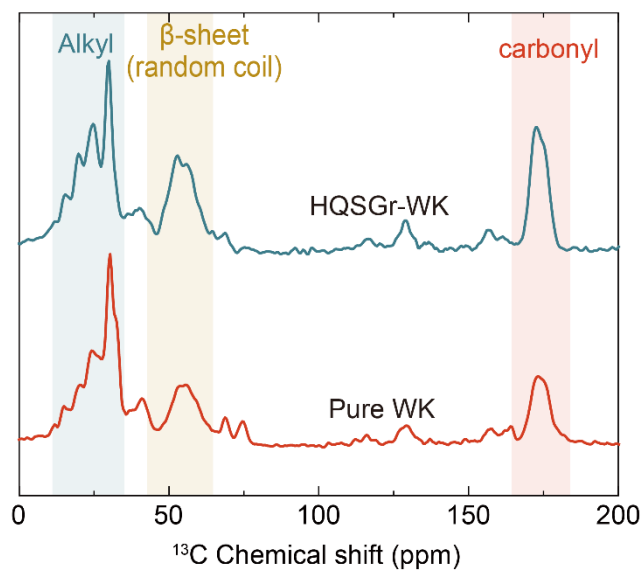


Figure S10. ^{13}C NMR full spectra between pure WK and HQSGr-WK hybrid dispersions.

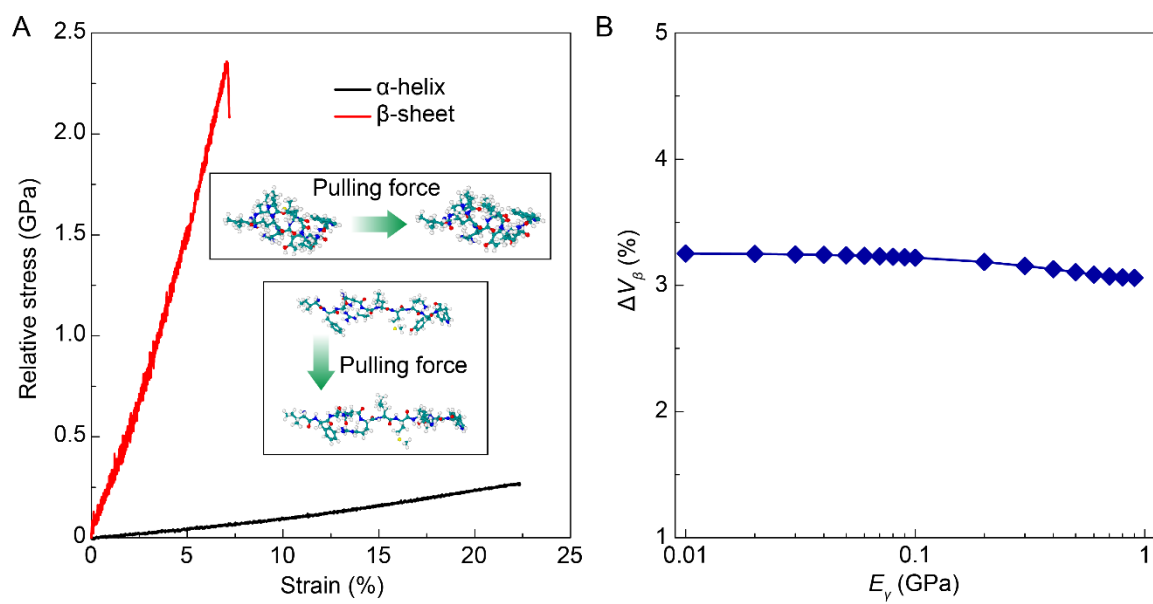


Figure S11. A) Stress-strain curves of α -helix and β -sheet. B) Effect of modulus of amorphous region on the increase of β -sheet content.

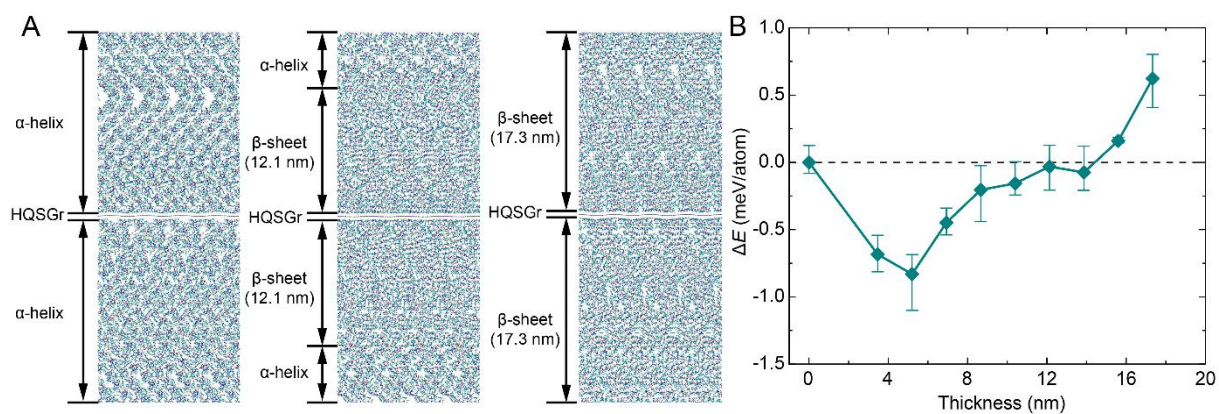


Figure S12. A) Snapshots for keratins with different ranges of β -sheets onto graphene. B) Potential energy per atom for keratins with different ranges of β -sheets onto graphene with respect to that for full α -helices onto graphene.

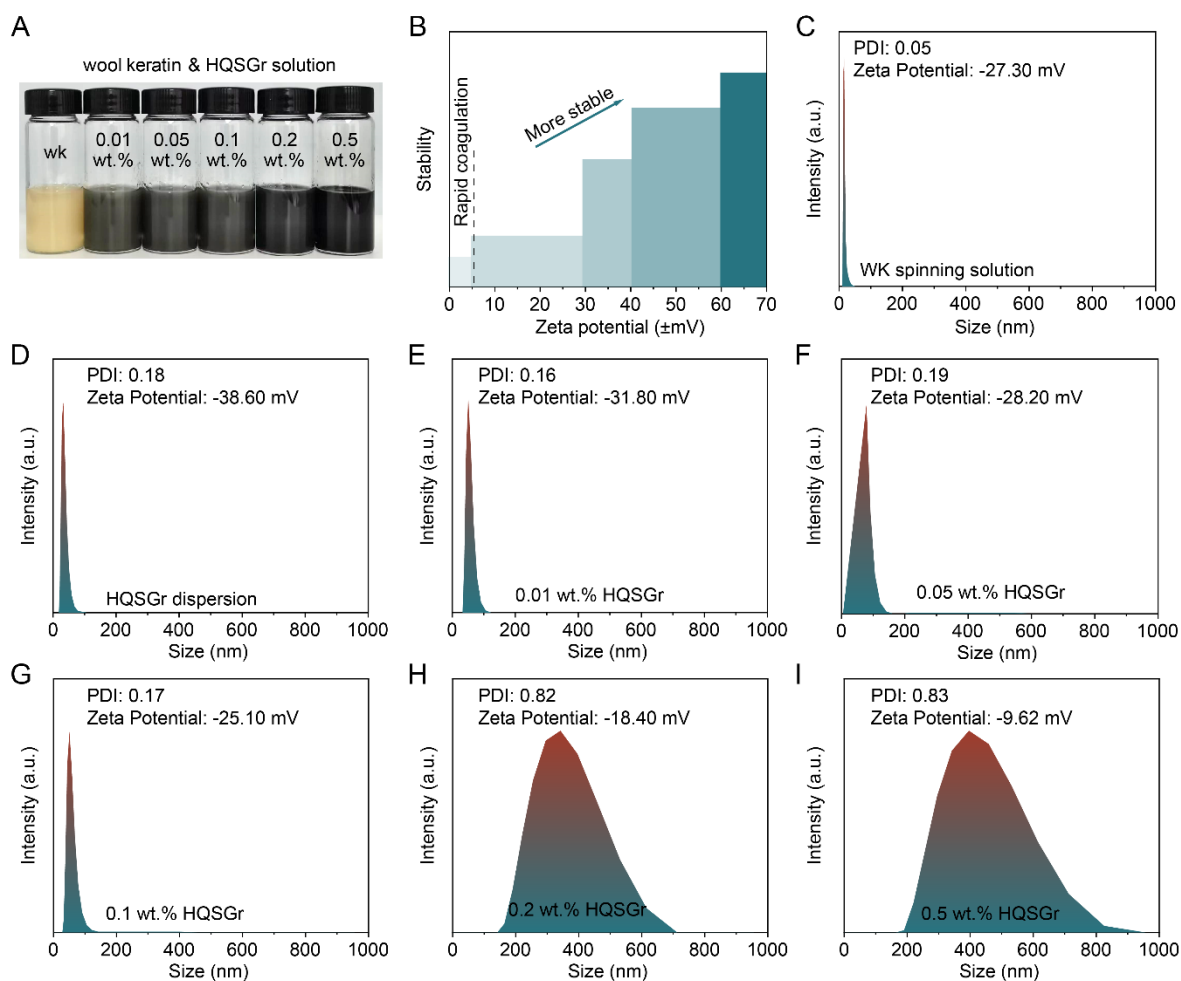


Figure S13. Effect of HQSGr addition on stability and homogeneity of composite spinning solution. A) Digital photographs of composite spinning fluids in different proportions. B) Relationship between Zeta potential value and stability of solution. The absolute value of the Zeta potential is proportional to the stability and dispersion of the solution. C-I) Zeta potential values and PDI values of spinning solutions with different addition ratios of HQSGr. PDI is the representative indicator of the average particle size in the dispersion, which negatively correlates to the stability and homogeneity of the mixed dispersion.^[2,3] It summarized the Zeta potential and PDI of WK, pure HQSGr and dispersions with different addition ratios of HQSGr. While the HQSGr ratio increases from 0.01 wt.% to 0.1 wt.%, the dispersion manifests Zeta potentials of -31.80, -28.20 and -25.10 mV and PDI values of 0.16, 0.19, and 0.17, close to those of -27.30, -38.60 mV and 0.049, 0.18 for pure WK and HQSGr dispersion. However, when the HQSGr ratio increases to 0.2 wt.%, or even 0.5 wt.%, the Zeta potential remarkably changes to -18.40 or -9.62 mV, while PDI value increases to 0.82 and 0.83.

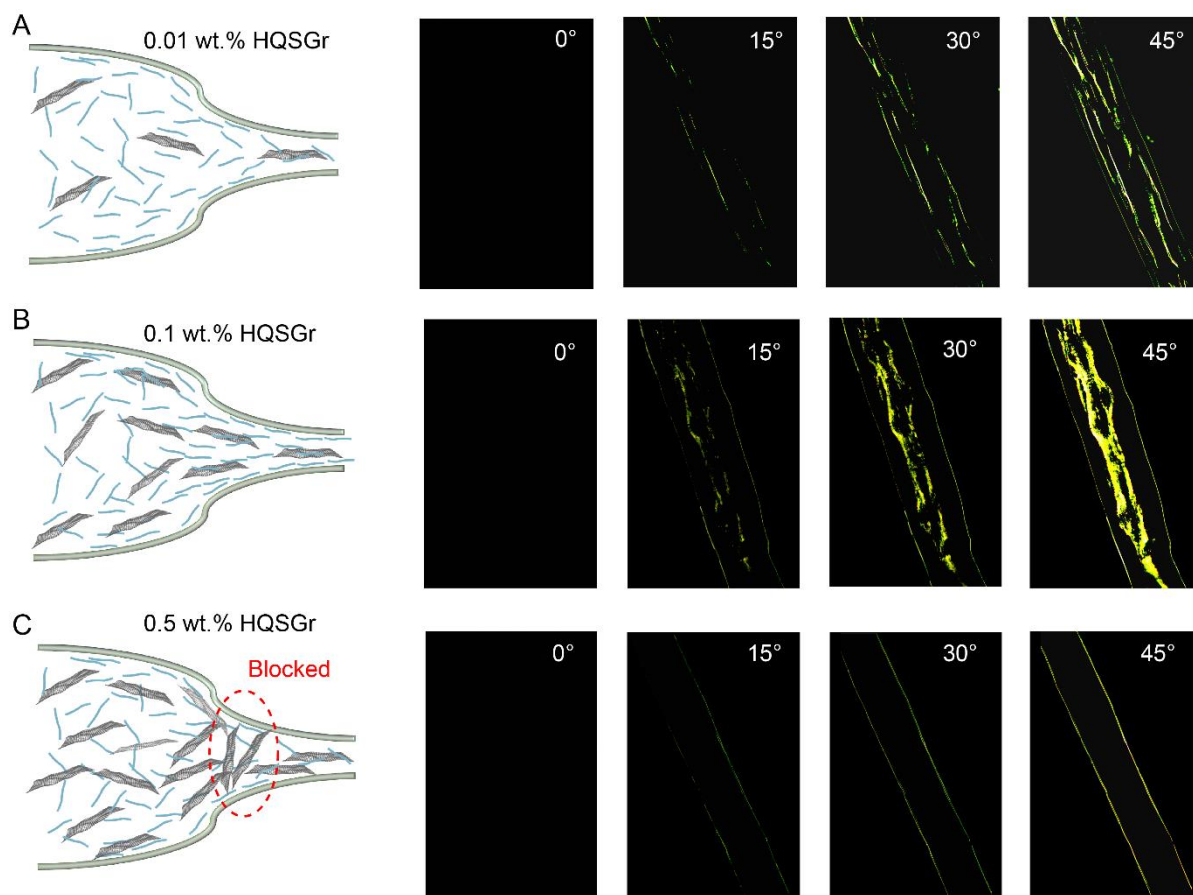


Figure S14. Effect of HQSGr addition on fiber crystallinity. A) Effect of trace HQSGr on fiber crystallinity. B) Effect of moderate HQSGr on fiber crystallinity. C) Effect of excess HQSGr on fiber crystallinity. Anisotropic birefringence characteristics can be analyzed qualitatively to obtain the change of fiber crystallinity. Proper amount of HQSGr can greatly improve the fiber crystallinity.

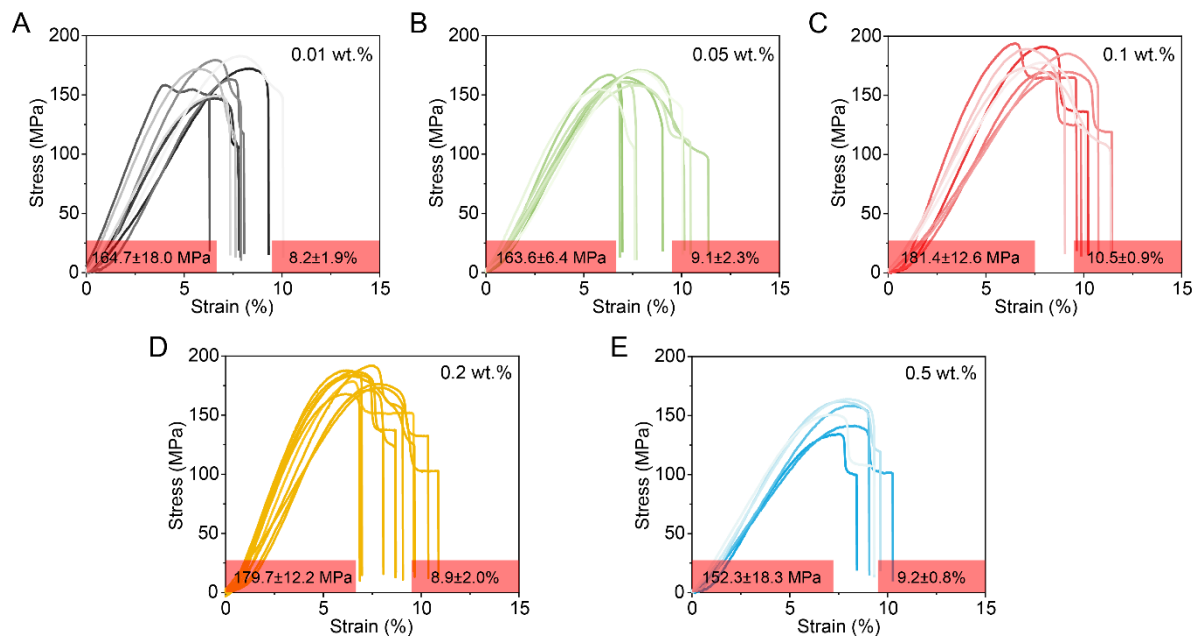


Figure S15. Stress-strain curves of HQSGr-RWKF with different HQSGr addition ratios.

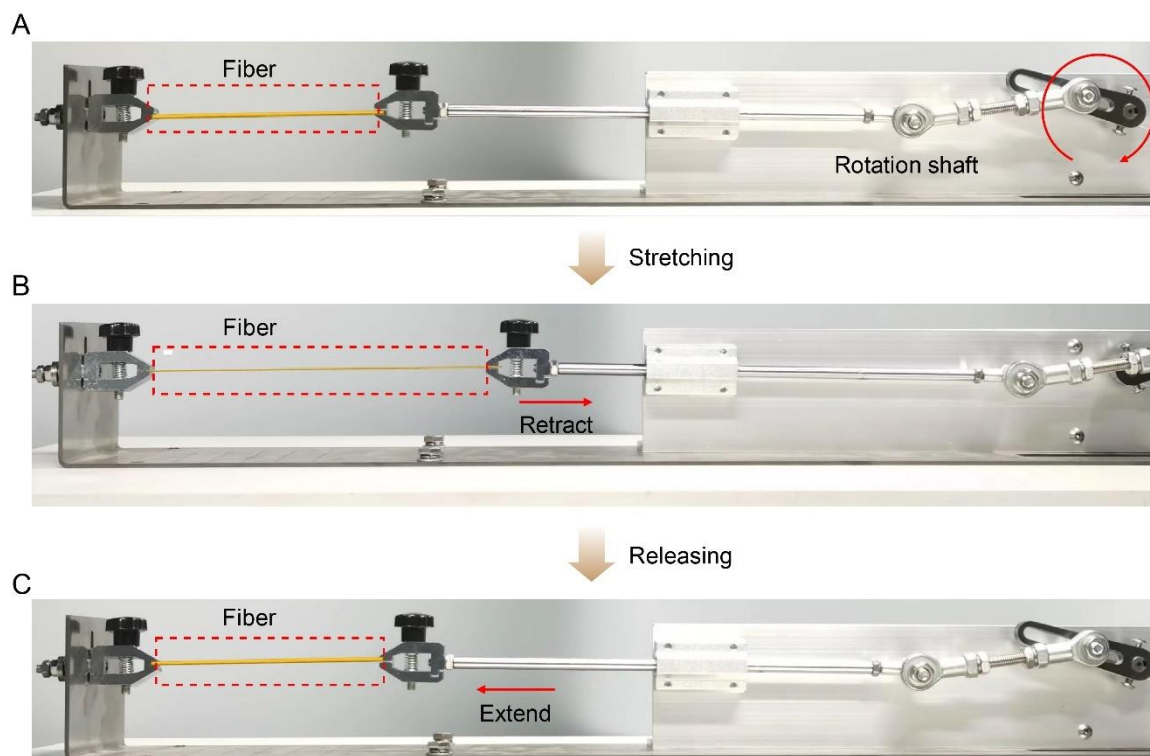


Figure S16. Mechanical training process by means of a self-built mechanical training device.

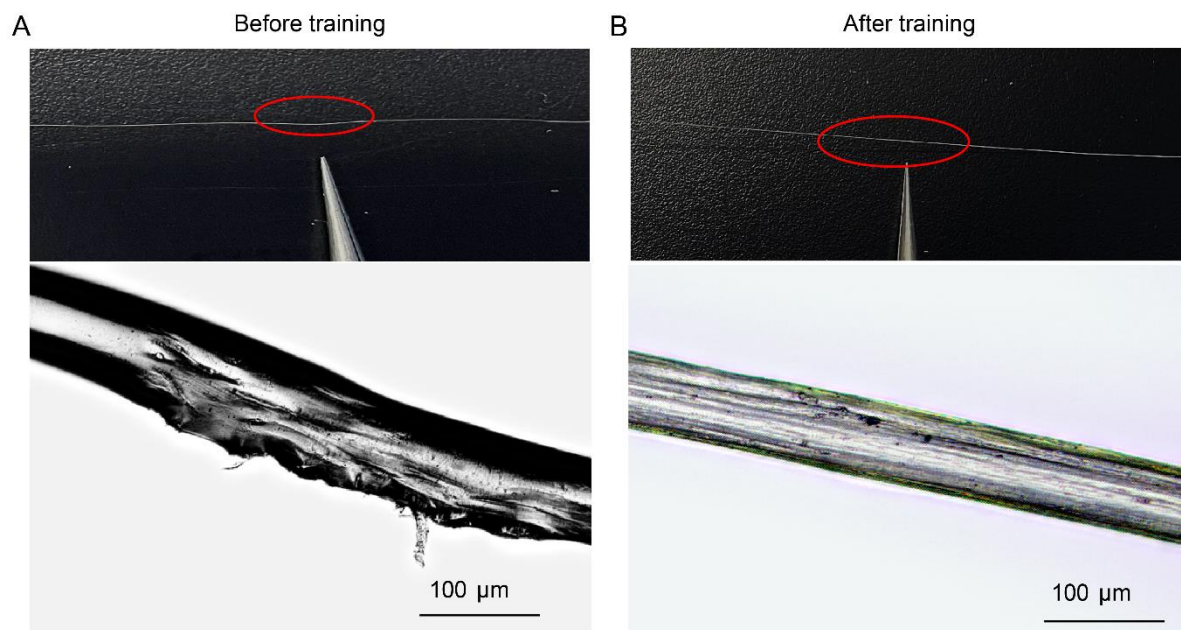
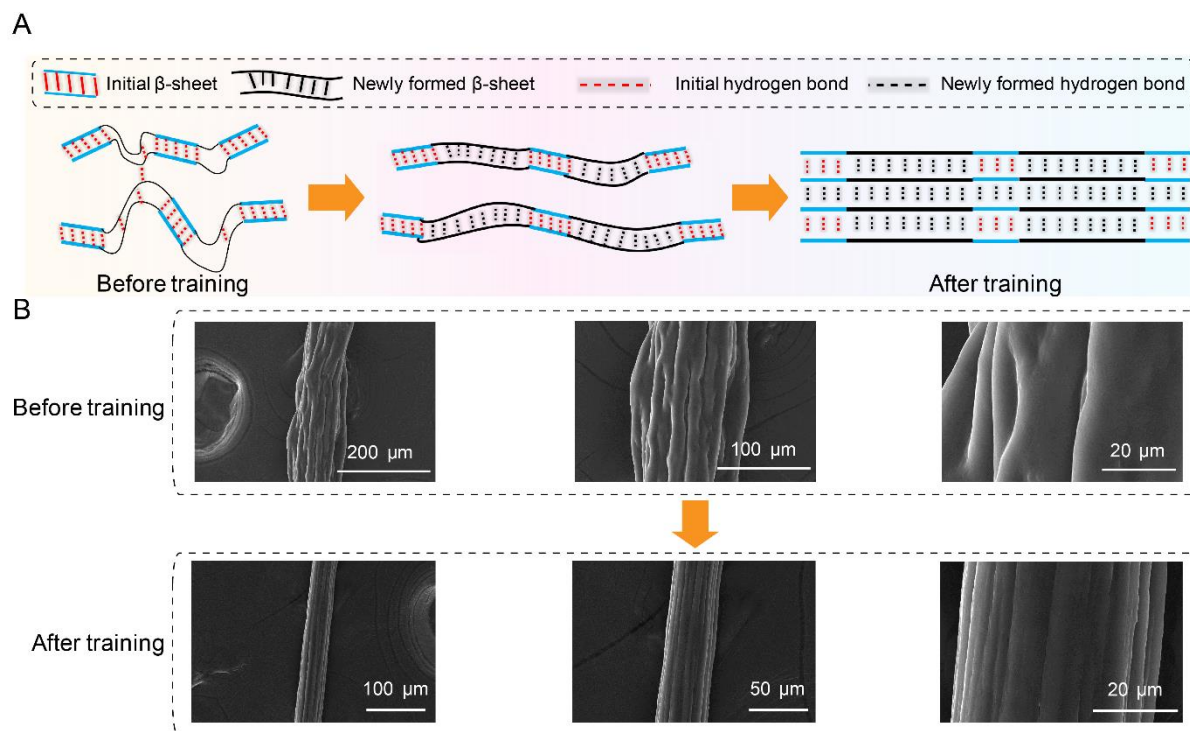


Figure S17. Effect of mechanical training on hybrid keratin fiber surface defects. A) Hybrid keratin fiber surface with microdefects before mechanical training under light microscope. B) Hybrid keratin fiber surface with disappeared microdefects after mechanical training under light microscope.



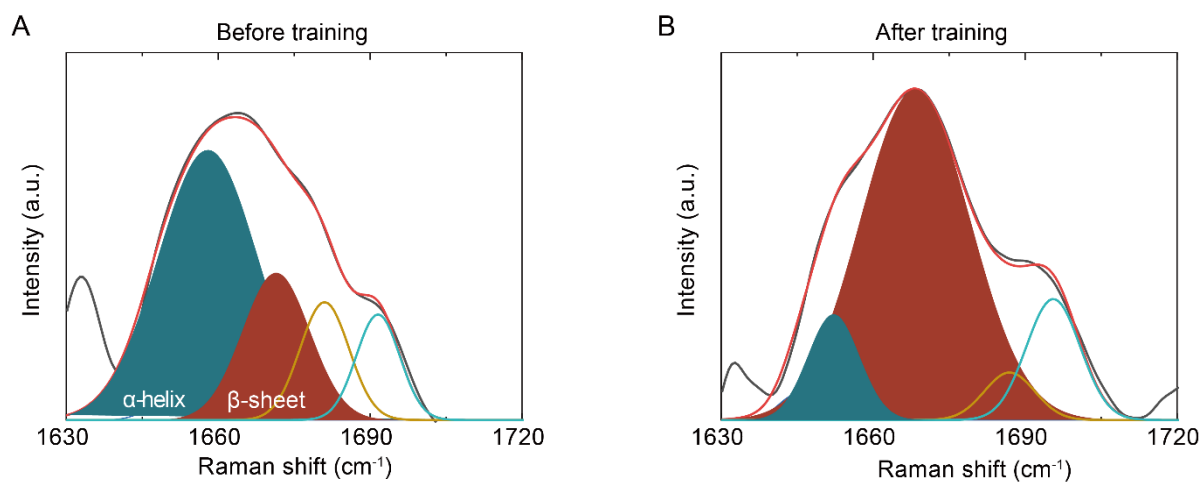


Figure S19. Deconvolved Raman spectra of hybrid keratin fiber before and after training.

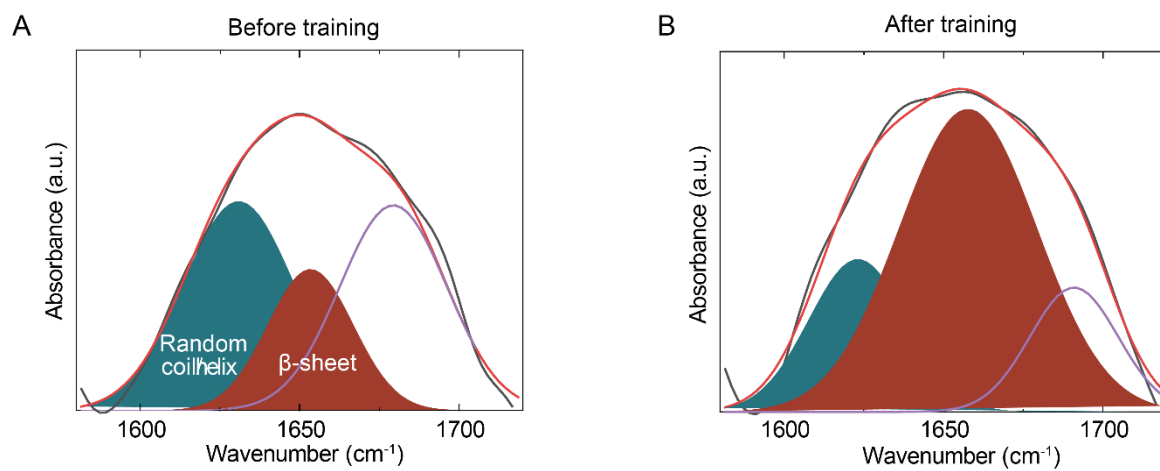


Figure S20. Deconvoluted FT-IR spectra of hybrid keratin fiber before and after training.

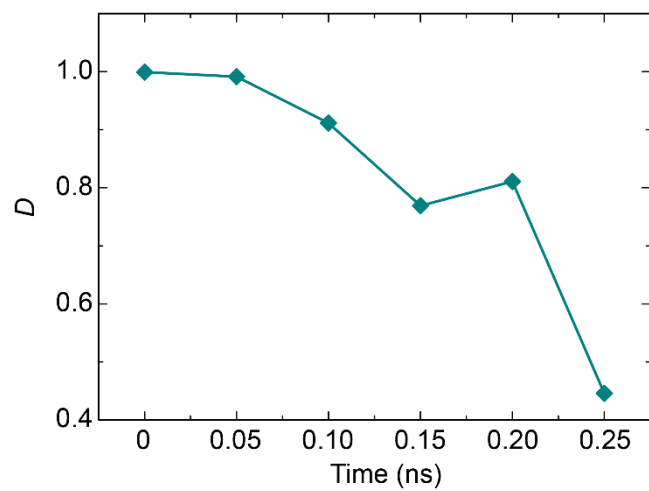


Figure S21. Evolution of β -sheet coiling into α -helix while contacting moisture. D stands for the transition degree from α -helix to β -sheet.

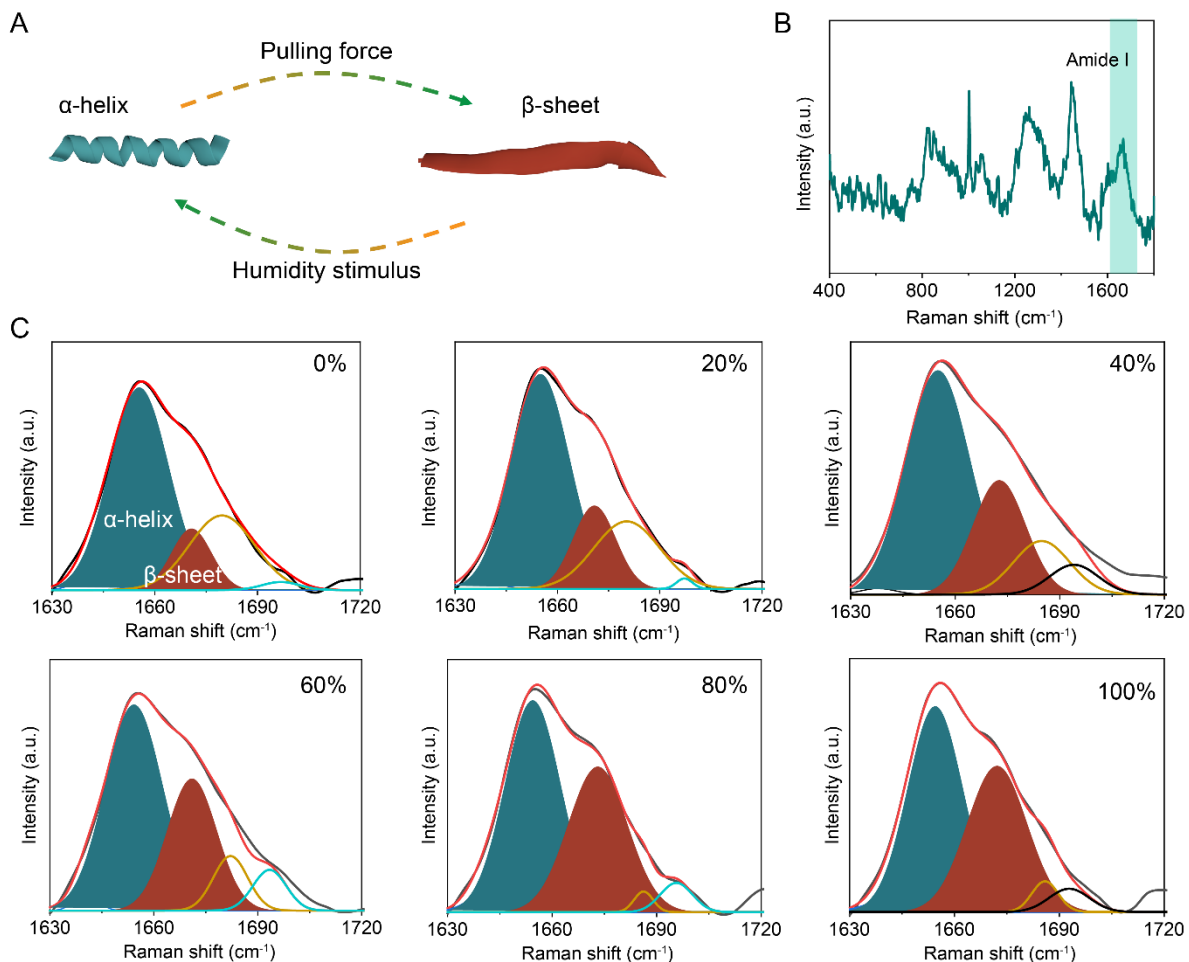


Figure S22. Actuation mechanism of RWKF. A) Schematic diagram of actuation mechanism of RWKF. B, C) Deconvoluted amide bands of Raman spectra of fibers at different stretching stages. With the continuous stretching, the area of the β -sheet deconvolution peak increases, indicating that the content of β -sheet increases gradually.

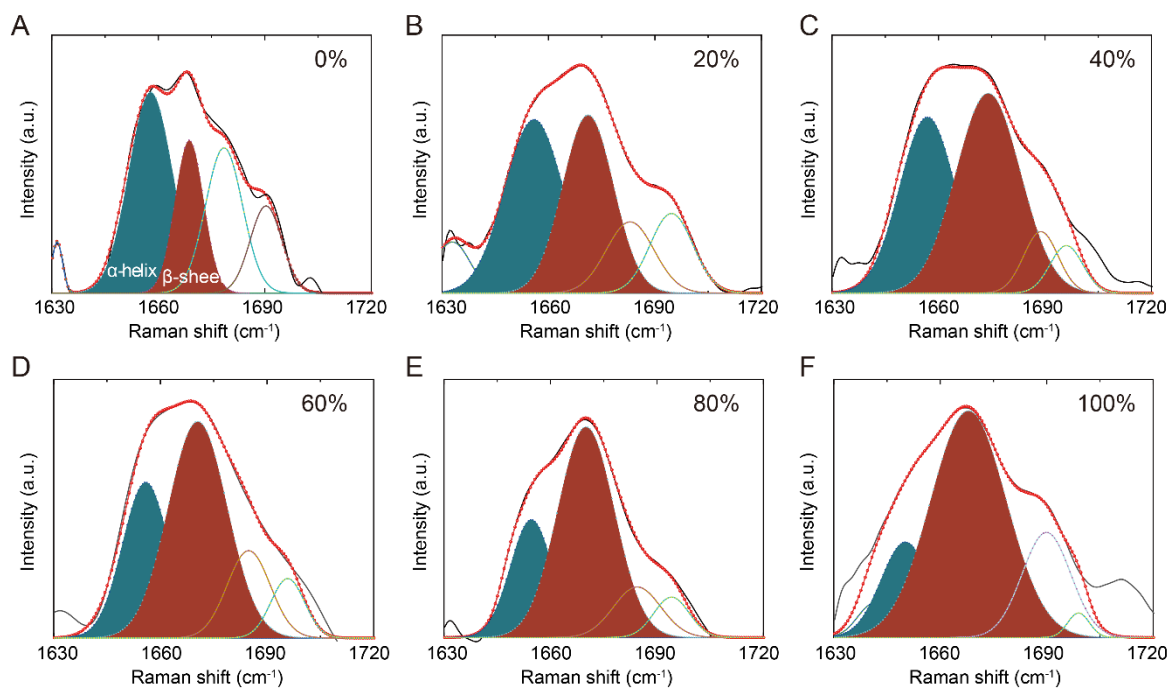


Figure S23. Deconvolved amide bands of Raman spectra of M-HQSGr-RWKF at different stretching stages. With the continuous stretching, the area of the β -sheet deconvolution peak increases, indicating that the content of β -sheet increases gradually.

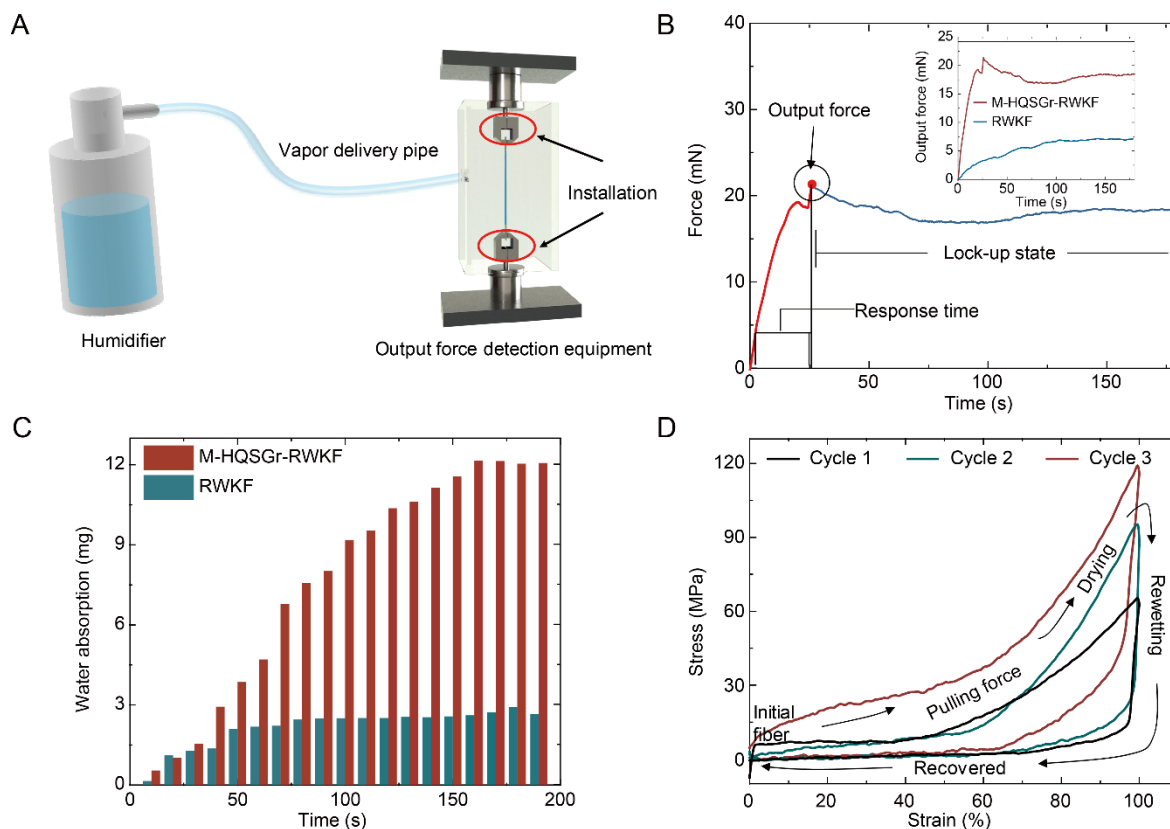


Figure S24. Measurement of actuation performance for M-HQSGr-RWKF artificial muscle. A) Self-built device about the output force testing. B) Time-force curve of M-HQSGr-RWKF artificial muscle. The inset shows the comparison of RWKF and M-HQSGr-RWKF artificial muscles. The whole curve conveys three kinds of information: The response time of M-HQSGr-RWKF artificial muscle is from the starting point to the highest point; The highest point is the output force of M-HQSGr-RWKF artificial muscle; The following plateau area is the locked state of M-HQSGr-RWKF artificial muscle. At this time, no external energy input is needed, and M-HQSGr-RWKF artificial muscle can maintain the contraction state and continue to work. C) Water absorption of RWKF and M-HQSGr-RWKF within 200 s. Put the fiber (100 mg) into a box with the humidity of 100% and the temperature of 26 °C. D) Stress-strain curves of fiber during the cyclic tension-recovery process. Once the strain reaches 100% during the cycle, the humidity stimulation was applied, inducing the fiber recovery to its initial state.

Table S1. Tensile strength comparison of various keratin based fibers.

Materials	Tensile strength (MPa)	Refs.
WKA	101	[4]
FKA	75	[5]
WKA/GO-PEG	157	[6]
FKA	138±30.5	[7]
FKA	160.7	[8]
WKA	137.18	[9]

Table S2. Details of the deconvolution analysis of Raman spectra using Peak fit software.

Operation steps	Specific parameters
Data section	1630-1725
Baseline adjustment	Algorithm: 2nd Deriv Zero Linear: 3.0% Lin
Smooth	Algorithm: Gauss Convol Level: 4.0%
Deconvolve Gauss IRF	Resp Fn Width: FWHM 0.55319 Symmetric
AutoFit Peaks II Second Derivative	Baseline: No Baseline Smoothing: 1 Sm% Peak Type: Spectroscopy Gauss Amp AutoScan: 1.5 Amp% Vary Widths
Number of Peaks	Four

Table S3. This work is compared with the actuation indexes of various types of artificial muscles.

Muscle category	Materials	Strain (%)	Stress (MPa)	Work density (KJ/m ³)	Refs.
Natural muscle	Skeletal muscle (typical)	20	0.1	8	[10]
	Skeletal muscle (maximum)	>40	0.35	40	
Biomass artificial muscle	RWKF	>100	1.5	200	This work
	HQSGr-RWKF	>100	16.7	400.8	
	Spider silk	2.5	80	500	[11]
	Silk	70	3.2	172	[12]
Polymeric artificial muscle	Biomass lignin	40	1.5		[13]
	Nylon6,6	10	22		[14]
	Nylon6,6	20	50		[15]
	PEVA	68	0.55		[16]
	PAA	24	0.23		[17]
	PU+PANi	1.65	2.26	NA	[18]
Pneumatic artificial muscles	PPAM	38	0.16		[19]
	OV-PAM	90	0.04		[20]
CNTs artificial muscle	CNTs	1.3	11		[21]
	CNTs	5	37		[22]
	CNTs	3.5	10.8		[23]

Text S1. Further discussion of theoretical analysis

The RWKFs were divided into amorphous, α -helix and β -sheet regions, and the modulus of RWKFs (E_{c1} , 1.7 GPa) can be determined by the rule-of-mixture as

$$E_{c1} = E_{\alpha}V_{\alpha1} + E_{\beta}V_{\beta1} + E_{\gamma}V_{\gamma1} \quad , \quad (1)$$

where E_{α} , E_{β} and E_{γ} represent the Young's moduli of α -helix, β -sheet and amorphous regions, respectively. $V_{\alpha1}$, $V_{\beta1}$ and $V_{\gamma1}$ are the volume fractions of α -helix, β -sheet and amorphous regions in RWKFs, respectively. Considering that HQSGr can act as nucleating agents for transition from α -helix to β -sheet, the range of β -sheets onto graphene is expected to be far larger than its own size. The volume fractions of three regions will change accordingly with the addition of HQSGr, and thus the Young's modulus of HQSGr-RWKFs (E_{c2} , 3.2 GPa) can be deduced as

$$E_{c2} = E_{\alpha}V_{\alpha2} + E_{\beta}V_{\beta2} + E_{\gamma}V_{\gamma2} + E_gV_g \quad , \quad (2)$$

where $V_{\alpha2}$, $V_{\beta2}$ and $V_{\gamma2}$ are the volume fractions of α -helix, β -sheet and amorphous regions in HQSGr-RWKFs, respectively. E_g (1000 GPa) and V_g (0.055%) are the Young's modulus and volume fraction of HQSGr. To solve **Eq. (1)** and **Eq. (2)**, other formulas should be introduced based on the experimental results, that is,

$$V_{\alpha1} + V_{\beta1} + V_{\gamma1} = 1 \quad , \quad (3)$$

$$V_{\alpha2} + V_{\beta2} + V_{\gamma2} + V_g = 1 \quad , \quad (4)$$

$$\frac{V_{\beta1}}{V_{\alpha1}} = \frac{13}{87} \quad , \quad (5)$$

$$\frac{V_{\beta2}}{V_{\alpha2}} = \frac{7}{18} \quad . \quad (6)$$

Additionally, E_{α} (0.9 GPa) and E_{β} (32.0 GPa) can be obtained from atomistic simulations (Figure S11A). Considering that the modulus of amorphous region is undetermined, we investigated how it will affect the prediction by adjusting this value (0.01~0.9 GPa) and found a negligible effect (Figure S11B). With the above-mentioned experimental and simulated

results, the increase of V_β (ΔV_β) can be calculated as $3.2\% \pm 0.1\%$. Based on the volume fraction ratio and the thickness of graphene (0.34 nm), the range of β -sheets onto graphene is predicted as 9.8 ± 0.3 nm.

Text S2. Further discussion of atomistic simulations

To investigate the structural deformation between α -helix and β -sheet, the α -region (residue sequence number: 471-480, IFAQRLMKYW) of proteins (PDB ID: 5FOQ) from the Protein Data Bank was adopted for simulations based on experimental evidence of the amino acid residues.^[24] The atomic coordinate file for α -helix was provided in **Text S3**. The microstructural evolution of proteins was explored by atomistic simulations using the large-scale atomic/molecular massively parallel simulator (LAMMPS) package.^[25] The mechanical and structural properties of proteins have been successfully explored using this method.^[26-30] The interatomic interactions for graphene were described using the all-atom optimized potential.^[31] The CHARMM36 force field was used for the keratin, and the water molecule was represented by the TIP3P model.^[32] The interactions between water, graphene and keratin include both van der Waals and electrostatic terms. The former one was described by the 12-6 Lennard-Jones potential truncated at 1.2 nm. The particle-particle particle-mesh algorithm was used to compute the long-range Coulomb interactions.^[33] The time step of Verlet algorithm was set to 1 fs in the simulations. For all simulations, the constructed structures were fully energy minimized using a conjugate gradient algorithm. To investigate the effect of graphene on keratin, an α -helix was placed on the fixed monolayer graphene, and periodic boundary conditions were employed along the in-plane directions with a vacuum layer over 10 nm along the out-of-plane direction. The system was equilibrated at 300 K for 2 ns to achieve the equilibrium of protein. To distinguish the folded α -helix and unfolded β -sheet, the radius of gyration (R_g) was utilized to characterize the compactness of the system. As presented in Figure S9, R_g rapidly increased from 6.2 Å to 9.5 Å and remained stable for the duration of the simulations, indicating that α -helix spontaneously uncoils into β -sheet. The trend of R_g demonstrates the stability of β -sheet onto monolayer graphene. In simulations investigating the effect of water on keratin, the model was formed by adding water molecules around the β -sheet, and the system was equilibrated at 300 K for 1 ns to equilibrate the

structure.

To balance the computational accuracy and efficiency, a uniaxial tensile velocity of 1 m/s was employed during the tensile test for both α -helix and β -sheet. A maximum strain limit of 20% was imposed on all bonds, and failure occurred when the strain of bonds was achieved. The evolution of strain and relative stress (the stress with respect to the pre-stress) shows that the α -helix exhibits relatively low load resistance, whereas the β -sheet exhibits relatively high load resistance (**Figure S11**).

To investigate the behaviors of structures of β -sheets onto graphene with respect to that of full α -helices onto graphene, a wide range of α -helices (~ 17.0 nm) were initially placed onto monolayer graphene, with periodic boundary conditions applied along all directions. After equilibrating the proteins at a temperature of 300 K and pressure of 1 atm for a duration of 0.1 ns, the system was subjected to energy minimization, and the final potential energy was recorded. Subsequently, α -helices close to the graphene were progressively translated into β -sheets. The values of potential energy per atom for all systems relative to the potential energy of full α -helices onto graphene were compared (**Figure S12**) and analyzed for recognizing the energetically favorable range.

Text S3. Atomic coordinate file for α -helix

193

	87.858	58.508	135.658									
O	14.714	4.563	23.929	H	9.124	10.022	24.673	H	4.713	15.850	29.662	
C	14.047	5.605	23.954	N	9.726	9.262	24.912	N	5.509	15.688	29.086	
H	14.164	9.218	16.497	O	11.781	8.473	25.389	O	4.257	16.148	27.275	
C	14.369	8.984	17.532	C	11.042	9.398	25.056	C	5.342	15.835	27.778	
H	16.451	9.335	17.304	H	13.968	13.804	27.764	H	6.767	16.490	26.314	
C	15.658	9.059	17.981	H	12.890	12.538	28.445	H	7.411	15.425	27.607	
H	12.308	8.565	17.989	H	12.949	14.169	29.198	C	6.557	15.580	26.913	
C	13.314	8.614	18.381	C	12.975	13.625	28.229	H	6.053	13.485	26.598	
H	12.707	8.036	20.342	S	11.662	14.168	27.161	H	5.573	14.575	25.273	
C	13.540	8.315	19.711	H	11.457	13.556	24.843	C	6.382	14.374	26.013	
C	14.849	8.391	20.205	H	13.053	13.107	25.528	H	8.481	13.898	25.880	
C	15.889	8.766	19.322	C	11.961	13.119	25.732	C	7.638	14.017	25.210	
H	17.940	8.949	19.656	H	11.942	11.249	26.852	H	7.322	15.838	24.259	
N	17.059	8.760	20.033	H	10.362	11.747	26.195	N	7.982	15.089	24.287	
H	17.521	8.282	22.127	C	11.452	11.707	25.964	O	9.896	14.120	23.610	
C	16.786	8.396	21.341	H	12.672	10.651	24.539	C	9.091	15.048	23.554	
C	15.445	8.156	21.495	C	11.618	10.777	24.756	H	10.893	17.129	23.791	
H	15.463	7.656	23.615	H	10.541	12.219	23.707	H	9.241	17.795	24.085	
H	14.039	8.575	23.051	N	10.983	11.336	23.563	H	10.127	18.212	22.578	
C	14.728	7.743	22.785	O	11.640	9.656	22.196	C	9.929	17.398	23.307	
H	14.264	5.862	21.860	C	11.007	10.697	22.392	H	10.042	15.873	21.863	
C	13.898	6.459	22.687	H	9.496	11.119	18.687	C	9.314	16.213	22.591	
H	12.282	7.748	22.426	H	11.140	11.390	18.005	H	7.805	17.562	22.046	
N	12.506	6.777	22.402	H	9.742	12.299	17.349	N	8.074	16.607	21.923	
O	11.875	4.630	22.107	C	10.188	11.888	18.280	O	7.688	14.570	21.039	
C	11.610	5.833	22.131	H	12.332	13.662	18.543	C	7.363	15.745	21.204	
H	7.151	9.460	17.988	H	11.394	14.932	19.413	H	10.094	17.322	16.565	
C	7.334	8.561	18.558	H	10.913	14.433	17.750	C	9.230	16.770	16.908	
H	9.359	9.078	18.955	C	11.313	14.067	18.720	H	8.663	18.272	18.314	
C	8.581	8.345	19.119	H	9.413	13.445	19.549	C	8.413	17.307	17.895	
H	5.123	8.719	17.755	C	10.408	13.003	19.300	H	9.569	15.114	15.594	
O	5.108	7.841	18.142	H	12.046	12.109	20.439	C	8.937	15.529	16.366	
C	6.350	7.616	18.710	H	11.066	13.288	21.342	H	7.597	13.866	16.387	
H	5.819	5.721	19.553	C	11.001	12.454	20.606	C	7.831	14.833	16.810	
C	6.601	6.456	19.433	H	10.007	10.554	20.536	H	6.140	14.832	18.135	
H	8.045	5.332	20.523	C	10.204	11.326	21.269	C	7.011	15.379	17.800	
C	7.850	6.249	19.985	H	8.792	12.790	21.714	C	7.305	16.613	18.363	
C	8.857	7.189	19.839	N	8.900	11.798	21.733	H	6.873	18.168	19.774	
H	10.836	6.376	19.739	O	8.161	9.729	22.227	H	5.470	17.490	18.897	
H	10.690	7.979	20.522	C	7.964	10.946	22.138	C	6.414	17.221	19.418	
C	10.222	6.973	20.448	H	5.074	9.922	17.267	H	5.489	15.434	20.304	
H	9.551	5.467	21.883	H	5.034	11.065	15.969	C	6.090	16.287	20.595	
C	10.210	6.325	21.829	N	4.798	10.797	16.892	H	5.219	17.987	21.421	
H	9.578	8.195	22.513	H	3.689	13.557	18.006	N	5.334	17.013	21.609	
N	9.747	7.271	22.850	H	4.250	13.195	16.392	O	4.981	15.233	22.957	
O	9.799	5.763	24.527	N	4.123	12.945	17.342	C	4.836	16.432	22.697	
C	9.572	6.906	24.124	C	4.357	11.704	17.751	H	-0.197	17.688	23.502	
H	6.072	9.011	28.630	H	4.309	10.432	19.363	H	0.461	19.268	22.935	
H	7.370	8.330	29.483	H	4.152	11.365	19.020	H	-0.133	19.090	24.626	
H	5.786	8.161	30.071	N	3.915	13.314	19.696	C	0.403	18.573	23.800	
N	6.373	8.204	29.213	H	2.580	12.181	20.160	H	2.302	19.078	24.611	
H	6.527	6.104	29.091	C	3.684	12.282	20.050	H	1.682	17.472	25.110	
H	5.146	6.831	28.184	H	4.122	12.802	22.107	C	1.778	18.166	24.245	
C	6.225	6.946	28.430	H	3.997	11.049	21.865	H	1.885	15.520	23.643	
H	8.153	6.972	27.408	C	4.355	11.986	21.384	H	2.705	15.633	22.043	
H	6.880	6.037	26.552	H	6.129	11.173	20.414	H	1.054	16.300	22.251	
C	7.068	6.956	27.153	H	6.237	12.888	20.877	C	2.036	16.165	22.752	
H	5.677	8.226	26.068	C	5.852	11.896	21.213	H	2.699	18.247	22.306	
H	7.048	9.090	26.840	H	6.069	10.799	23.060	C	2.626	17.513	23.148	
C	6.768	8.165	26.286	C	6.606	11.553	22.497	H	4.101	16.890	24.621	
H	7.146	7.299	24.327	H	6.308	13.572	23.025	C	4.068	17.350	23.641	
H	7.342	9.069	24.416	N	6.750	12.737	23.344	H	4.150	19.419	23.506	
C	7.536	8.121	24.969	O	7.894	11.649	24.957	N	4.717	18.646	23.781	
H	9.297	7.644	26.098	C	7.440	12.694	24.484					

C 9.058 7.976 25.095 | H 6.403 15.444 29.446 |

Description of Movies S1 to S4

Movie S1. Atomistic simulations show the stretching of the α -helix under pulling force.

Movie S2. Atomistic simulations show β -sheet spontaneously transforms to helical structure in aqueous environment.

Movie S3. M-HQSGr-RWKF drives petal motion stimulated by humidity.

Movie S4. M-HQSGr-RWKF drives robot arm stimulated by humidity.

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