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# **Electromechanically Actuated MXene Nanotubes for Tunable Mass** Transport

Bozhao Wu,<sup>§</sup> Yuanpeng Yao,<sup>§</sup> Ke Zhou, Ze Liu,<sup>\*</sup> and Enlai Gao<sup>\*</sup>



analyses. Finally, we probe the transport behaviors of a molecule test case (neopentane,  $C_{s}H_{12}$ ) passing through electromechanically actuated MNTs and demonstrate that the tunability of sieving diameters endows MNTs with the capability of tunable mass transport. These findings provide a feasible solution for the development of tunable nanochannels.

# INTRODUCTION

Solid-state actuator materials that convert external stimuli into mechanical responses<sup>1-4</sup> are of practical interest for applications, such as micro- and nanoelectromechanical devices, artificial muscles, robotics, resonators, sensors, and switches. Although developing actuator materials has attracted considerable attention, classical actuator materials, including electroactive ceramics, polymers, and shape memory alloys, have shortcomings, such as small strokes and unpredictable deformation,<sup>5,6</sup> which limit their applications. Electromechanical actuation materials provide a promising route to address this issue.<sup>7-10</sup> For example, Baughman<sup>7</sup> found that carbon nanotube sheets exhibit remarkable actuation performance when immersed in an aqueous electrolyte. Afterward, firstprinciples calculations predicted dimensional changes of carbon nanotubes as a function of charge injection.<sup>8</sup>

underlying mechanism behind this high actuation performance of

MNTs and planar Sc<sub>2</sub>C is revealed by atomic- and electronic-scale

Recently, the discovery of two-dimensional materials (2DMs) has accelerated the development of micro- and nanoscale material-based actuators. The actuation performance of numerous 2DMs, such as graphene and its oxide,<sup>10</sup> phosphorene,<sup>13</sup> transition-metal dichalcogenides,<sup>14,15</sup> and MXenes,<sup>16–18</sup> has been investigated by experiments and theoretical calculations. On the experimental side, a graphene-based electromechanical resonator exhibits actuated vibrations with fundamental resonant frequencies in the megahertz range under a direct current voltage.<sup>19</sup> A MXene  $(Ti_3C_2T_x)$ -based actuator shows changes in curvature and strain up to 0.038 mm<sup>-1</sup> and 0.26% under a low voltage.<sup>18</sup> On the theoretical side, Liu et al.<sup>12</sup> found that the phase transition in graphene oxide provides a maximum recoverable stroke of

14.5%. More recently, it was predicted that phosphorene exhibits in-plane anisotropic strokes with a maximum actuation strain of 36.6%,<sup>13</sup> while Ti<sub>2</sub>C MXene boasts in-plane isotropic strokes with a maximum actuation strain of 27.4%.<sup>16</sup> Recently, experimental evidence demonstrated the formation of scrolls from planar  $Ti_3C_2$ ,<sup>20</sup> and the stability of MXene nanotubes (MNTs) also has been predicted by density functional theory (DFT) and density functional-based tight binding calculations.<sup>21,22</sup>

0.50

Diffusion coordinate

0.25

0.75

Considering that nanotubes can be formed by rolling up 2DMs, we wonder whether nanotubes prepared by rolling up responsive 2DMs would exhibit interesting actuation performance. Moreover, if the diameter of these nanotubes can be changed by an external stimulus, this responsive nanochannel can be highly promising for tunable mass transport. Tunable mass transport is of fundamental importance not only in separation-based applications<sup>23–25</sup> but also in biological sensing,<sup>26</sup> drug delivery,<sup>27,28</sup> catalysis,<sup>29,30</sup> nanofluidics,<sup>31,32</sup> proton transport,<sup>33</sup> and energy harvesting.<sup>34</sup> Responsive nanochannels with tunable sieving diameters are the best candidates for such applications.<sup>35–37</sup> To date, stimuli, such as heat,<sup>38</sup> environmental pH,<sup>39,40</sup> ions/molecules,<sup>41,42</sup> and light,<sup>43</sup>

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![](_page_1_Figure_3.jpeg)

**Figure 1.** Structures of planar Sc<sub>2</sub>C and MNTs. (a,b) Top and side views of planar Sc<sub>2</sub>C with the unit cell in the red dashed lines. (c,d) Side and top views of MNT-14. *D*, *L*,  $B_{1-4}$ , and  $\theta_{1-2}$  are the diameter, axial length, bond length, and angle of MNT-14, respectively. Panel (d) provides the enlarged side and top views of panel (c) within the blue dashed lines.

MNTs	D (Å)	L (Å)	$B_1$ (Å)	$B_2$ (Å)	$B_3$ (Å)	$B_4$ (Å)	$\theta_1 \; ({ m deg})$	$\theta_2 ~({\rm deg})$
MNT-6	9.02	3.42	2.24	2.37	2.35	2.23	116.74	77.66
MNT-10	16.12	3.33	2.28	2.35	2.28	2.21	109.17	81.60
MNT-14	23.30	3.31	2.29	2.33	2.26	2.21	105.30	83.91

Table 1. Structural Parameters of MNTs

have been used to produce controllable responses of nanochannels, but challenges remain, particularly in terms of stimulus complexity (e.g., solutions and ions) and response uncontrollability (e.g., low durability and response rate).<sup>36</sup>

Herein, we computationally investigate the actuation performance of  $Sc_2C$  MNTs in response to charge injection. Our results show that MNTs exhibit high electromechanical actuation performance with a maximum radial actuation strain of 26.8% while maintaining sufficient structural integrity under electromechanical loads. Insights into atomic and electronic structures reveal the underlying mechanism for this behavior. Finally, we demonstrate that the tunability of the diameter endows MNTs with the capability of tunable mass transport by passing a molecule ( $C_5H_{12}$ ) through an MNT with various actuated diameters.

### COMPUTATIONAL METHODS

First-principles calculations were performed under the framework of DFT as executed in the Vienna ab initio simulation package.<sup>44,45</sup> The generalized gradient approximation<sup>46</sup> of the Perdew–Burke–Ernzerhof functional<sup>47</sup> was used for the exchange and correlation interactions of electrons. Projector augmented wave potentials were used to treat ion-electron interactions.<sup>48</sup> Considering the dispersion interactions, van der Waals corrections using the DFT-D3 method were adopted in all calculations.<sup>49</sup> Monkhorst–Pack grid *k*-points<sup>50</sup> with densities greater than 40 Å were used for Brillouin zone sampling. The convergence test was performed to verify the rationality of the selected energy cutoff. Figure S1c,d demonstrates that the energy cutoff of 400 eV provides a good balance between computational accuracy and cost for the calculations of the electromechanical performance of planar  $Sc_2C$  and MNTs. Hence, the energy cutoff was set at 400 eV in all the calculations. All structures were fully relaxed using a conjugate gradient algorithm with a convergence criterion less than 0.01 eV/Å for the force on each atom. On calculating the electromechanical actuation performance of planar  $Sc_2C$  and MNTs, the injected charges were compensated using a jellium background charge to maintain charge neutrality in the computational cell. Unless otherwise noted, a vacuum layer of thickness greater than 70 Å was adopted to eliminate electrostatic interactions.<sup>13,16</sup>

### RESULTS AND DISCUSSION

Structures of Planar Sc<sub>2</sub>C and MNTs. Similar to rolling up graphene sheets into carbon nanotubes, MNTs can be constructed by rolling up planar  $Sc_2C$  (Figure 1a,b). Specifically, structural optimization was performed on the unit cell of planar Sc<sub>2</sub>C within the red dashed lines, which yields lattice parameters a = 5.71 Å and b = 3.30 Å and interatomic parameters B = 2.26 Å and  $\theta = 93.59^{\circ}$ . Afterward,  $6 \times 1$ ,  $10 \times 1$  and  $14 \times 1$  supercells of planar Sc<sub>2</sub>C are constructed and rolled into MNTs with diameters of 0.9-2.3 nm, named MNT-6, MNT-10, and MNT-14, respectively (Figures 1c and S1a,b). Unless otherwise mentioned, the diameter of an MNT refers to its inner diameter (D), as illustrated in Figure 1c. Table 1 lists the structural parameters of MNT-6, MNT-10, and MNT-14 (Figure 1c,d). In contrast to uniform bond length and angle of planar Sc<sub>2</sub>C, the bond length  $(B_{1-4})$  and angle  $(\theta_{1-2})$  of MNTs alternate, since bending-induced tension in the outer atomic layer and compression in the inner atomic layer of MNTs disrupt the

![](_page_2_Figure_3.jpeg)

**Figure 2.** Plotted ELF graphs of (a) MNT-14 and (b) planar  $Sc_2C$  before and after charge injection. The ELF graph of MNT-14 shown on the cross-sectional plane with the distance of *L* from the origin. For planar  $Sc_2C$ , the ELF graph of a supercell ( $3 \times 1 \times 1$ ) shown on the (010) plane with a distance of lattice *b* from the origin. (c,d) Actuation performance of MNTs and planar  $Sc_2C$  in response to charge injection. (c) Radial and axial actuation strain of an MNT-14 and (d) actuation strain of a planar  $Sc_2C$  along the armchair and zigzag directions.

symmetry of planar Sc<sub>2</sub>C.<sup>16</sup> In addition, this alternation of the bond length and angle decreases as the bending of the MNTs decreases (Table 1). Considering the thermodynamics, ab initio molecular dynamics (AIMD) simulations were carried out to investigate the stability of MNTs. The temperature of 298 K was controlled using an Andersen thermostat. During the whole AIMD simulations of 10 ps, the evolution of temperature and system energy is gentle (Figure S2a) and the MNT upholds its structural integrity with only slight corrugation because of thermal fluctuation (Movie S1). Considering the kinetics, the most likely instability for nanotubes is the collapse. The bending stiffness  $(K_{\rm b})$  of planar Sc<sub>2</sub>C was calculated using  $E_{diff} = K_b/(2r^2)$ ,<sup>51</sup> in which  $E_{diff}$  is the energy difference per unit area between planar and circular  $Sc_2C$  and *r* is the radius of circular  $Sc_2C$ . By fitting the relation between  $E_{\text{diff}}$  and r (Figure S2b), the calculated  $K_{\text{b}}$  of planar  $Sc_2C$  is 3.75 ± 0.10 eV. Previous work demonstrated that the single-wall carbon nanotube exists at a maximum diameter of 2.6 nm, in which the energy for a round and collapsed nanotubes is the same.<sup>52</sup> Since the bending stiffness of planar  $Sc_2C$  is much larger than that (1.4 eV) of planar graphene,<sup>53</sup> it can be inferred that the investigated MNTs (diameter ranging from 0.9 to 2.3 nm) in this work would not collapse.

Structural Integrity of Planar Sc<sub>2</sub>C and MNTs under Electromechanical Loads. Structural integrity is of fundamental importance for applications, and the structural integrities of planar Sc<sub>2</sub>C and MNTs upon charge injection were examined by performing mechanical tests. The thickness of 5.6 Å was adopted for planar Sc<sub>2</sub>C, which is obtained from the interlayer spacing of bilayer Sc<sub>2</sub>C (Figure S3a). First, uniaxial tensile tests of charge-injected planar Sc<sub>2</sub>C were performed along the armchair and zigzag directions (Figure S3b), respectively, which indicate that the maximum charge injection for planar Sc<sub>2</sub>C maintaining sufficient structural integrity (no phase transition and strain to failure  $\geq 1\%$ ) is 0.20 e/atom. From the stress-strain curves in Figure S3b, it is noted that the Young's modulus of planar Sc<sub>2</sub>C is reduced by charge injection. The Young's modulus of pristine planar Sc<sub>2</sub>C is calculated to be 204 GPa on the average. Upon charge injection of 0.20 e/atom, the determined Young's modulus decreases to 37.5 GPa on the average. Similarly, the maximum charge injections of MNT-6, MNT-10, and MNT-14 are determined as 0.14, 0.12, and 0.11 e/atom, respectively (Figure S3d), and the charge-injected MNTs can maintain sufficient structural integrity below the maximum charge injection. Additionally, comparing with the Young's modulus (132.8 GPa) of pristine MNT-6, the Young's moduli (122.5 and 106.5 GPa) of MNT-6 upon charge injection of 0.06 and 0.14 e/ atom decrease by 7.8% and 19.8%, respectively. These results demonstrate the softening of planar Sc<sub>2</sub>C and MNTs by charge injection because of the depletion of electrons (hole injection) that weakens the chemical bonds.

Furthermore, the electron localization function (ELF) graphs of MNT-14 and planar Sc<sub>2</sub>C before and after charge injection are plotted in Figure 2a,b. Before charge injection, strong electron localizations with a high ELF value (0.8-0.9)occur around Sc and C atoms of MNT-14 (planar Sc<sub>2</sub>C), indicating the ionic binding of Sc-C bonds. After charge injection, the strong electron localizations around Sc and C atoms show a little change. For further discerning of the bonding characteristics between Sc and C atoms, the Bader charge analysis was conducted.<sup>54</sup> Before charge injection, Sc and C atoms of planar Sc<sub>2</sub>C lose and gain 1.203 and 2.406 electrons on the average, respectively. When 0.20 e/atom is injected, Sc and C atoms lose and gain 1.466 and 2.332 electrons on the average, respectively. For pristine MNT-14, the Sc atom in the inner and outer atomic layers loses 1.057 and 1.313 electrons on the average, respectively, and each C

![](_page_3_Figure_2.jpeg)

Figure 3. Evolution of interatomic parameters for (a) planar Sc<sub>2</sub>C and (b,c) MNT-14 as functions of charge injection. Change in (b) bond length  $(B_{1-4})$  and (c) angle  $(\theta_{1-2})$  of an MNT-14 upon charge injection.

atom gains 2.370 electrons. The different charge transfer of atoms in the inner and outer atomic layers is caused by the bending of the MNTs. After charge injection (0.11 e/atom), the Sc atom in the inner and outer atomic layers loses 1.302 and 1.445 electrons on the average, respectively, and each C atom gains 2.417 electrons. Although the electron localization between Sc and C atoms shows a slight change upon charge injection, the distance between Sc and C atoms significantly increases, indicating that the bonds (Sc-C) are weakened by charge injection. Notably, as shown in Figure 2a,b, before charge injection, electron localization with the medium ELF value also occurs between Sc atoms in the same atomic laver. indicating the covalent bonding between Sc atoms. After charge injection, the electron localization in MNT-14 (planar  $Sc_2C$ ) between Sc atoms shows a reduction, suggesting the weaker covalent binding between Sc atoms than that before charge injection. Hence, it can be concluded that the softening of planar Sc<sub>2</sub>C and MNTs by charge injection should be attributed to the weakened chemical bonds.

Electromechanical Actuation Performance. Next, we investigate the electromechanical actuation performance of MNTs upon charge injection. Notably, only hole injection was explored in this work since it was found that materials upon hole injection exhibit higher actuation performance than that upon electron injection.<sup>10,16</sup> The actuation performance of MNTs is characterized by the radial and axial strain that are defined as the changes in D and L for MNTs upon charge injection divided by the values of *D* and *L* for pristine MNTs, respectively. Similarly, the actuation strain of planar Sc<sub>2</sub>C is characterized as the change of in-plane lattice parameters after charge injection divided by their corresponding original values before charge injection. First, both the radial and axial strain of MNT-14 increase with increasing charge injection. Afterward, the radial actuation strain is increasingly larger than the axial actuation strain as the charge injection exceeds 0.04 e/atom. Finally, the axial strain drops as the charge injection exceeds 0.10 e/atom (Figure 2c and Movie S2). Upon a maximum charge injection of 0.11 e/atom, the radial and axial strain of MNTs reach 26.8% and 7.8%, respectively, indicating significant anisotropic actuation performance. In sharp contrast, planar Sc<sub>2</sub>C exhibits an in-plane isotropic actuation strain of 11.0% upon charge injection of 0.11 e/atom, and the maximum actuation strain of planar Sc<sub>2</sub>C is as high as 23.5%, when the hole of 0.20 e/atom is injected (Figure 2d). Additionally, we find that the radial actuation strain of MNT-6 and MNT-10 are lower than that of MNT-14 upon the same amount of charge injection (Figure S4a), indicating that the

increase in bending curvature would limit the radial actuation of MNTs.

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Mechanism for High Electromechanical Actuation Performance. To uncover the underlying mechanism behind the electromechanical actuation performance of the planar  $Sc_2C$  and MNTs, we track their interatomic parameters in response to charge injection. The evolution of interatomic parameters is explored (Figures 3 and S4b-e). As shown in Figure 3a, the interatomic parameters of planar  $Sc_2C$  increase with increasing charge injection. The isotropic actuation strain of planar  $Sc_2C$  can be derived as functions of the interatomic parameters<sup>16</sup>

$$\varepsilon = \frac{B\sin(\theta/2)}{B_0\sin(\theta_0/2)} - 1 \tag{1}$$

where  $B_0(B)$  and  $\theta_0(\theta)$  are the bond length and angle of planar Sc<sub>2</sub>C before (after) charge injection, respectively. By substituting the interatomic parameters (B and  $\theta$ ) into eq 1, the obtained actuation strain is found to be consistent with the directly measured values (Figure 2d). Because of bendinginduced symmetry breakdown, eq 1 is no longer applicable for MNTs. Compared with the change in bond length and angle in planar  $Sc_2C$  (Figure 3a), the change in bond length and angle in MNTs is very different (Figures 3b,c and S4b-e), resulting from the bending-induced symmetry breakdown of MNTs. As a small amount of hole is injected (less than 0.04 e/atom), Figure 3b shows that  $B_1$  and  $B_2$  slightly elongate (~1.2%), while  $B_3$  and  $B_4$  slightly shorten (~0.18%), and Figure 3c shows that the change of  $\theta_1$  (~1.6%) is larger than that (~0.08%) of  $\theta_2$ . Hence, the very small actuation strain of MNT-14 upon a small amount of charge injection (less than 0.04 e/atom) is dominated by the changes in  $B_1$ ,  $B_2$ , and  $\theta_1$ . As charge injection increases,  $B_3$  and  $\theta_2$  significantly increase. When charge injection increases to 0.11 e/atom, the changes of  $B_3$  and  $\theta_2$  reach about 24.9% and 25.2%, respectively, which are much larger than the change of other parameters. Hence, the maximum actuation performance of MNT-14 is dominated by the elongation of  $B_3$  in the outer atomic layer and the change of  $\theta_2$  in the inner atomic layer (Figure 1d). Additionally, the structural change of MNT-6 and MNT-10 as functions of charge injection (Figure S4b-e) exhibits similar evolution of interatomic parameters for these MNTs upon charge injection. The difference in radial actuation strain of MNTs with different diameters results from the change in interatomic parameters (Figures 3b,c and S4b-e). As the charge injection increases to above 0.04 e/atom, the change in interatomic parameters (especially  $B_3$  and  $\theta_2$ ) of MNTs with a

![](_page_4_Figure_3.jpeg)

**Figure 4.** Top (up) and side (down) views of the excess charge density distribution of planar  $Sc_2C$  and MNT-14. (a–d) Excess charge density distribution of charge-injected planar  $Sc_2C$  with the injection amount of (a) 0.05, (b) 0.10, (c) 0.15, and (d) 0.20 e/atom is plotted, and the corresponding iso-surface values are 0.0008, 0.0015, 0.0018, and 0.0018 e/Bohr<sup>3</sup>, respectively. Panels (e–h) are the excess charge density distribution of MNT-14 upon charge injection of (e) 0.01, (f) 0.06, (g) 0.09, and (h) 0.11 e/atom with isosurface values of 0.000195, 0.00145, 0.00165, and 0.001845 e/Bohr<sup>3</sup>, respectively. The yellow and blue colors represent excess electron and hole, respectively.

![](_page_4_Figure_5.jpeg)

**Figure 5.** MNT actuator for tunable mass transport. (a) Structures of an MNT-6 and a  $C_5H_{12}$ . The pink spheres represent H atoms. (b) Energy profiles of  $C_5H_{12}$  passing through a pristine and an electromechanically actuated MNT-6. (c) Atomic configurations of  $C_5H_{12}$  through MNT-6 at the diffusion coordinates of 0.00, 0.25, and 1.00 in (b).

large diameter is larger than that of MNTs with a small diameter, which results in the obvious difference in radial actuation strain for MNTs with different diameters.

To further explore the source of the electromechanical actuation performance upon charge injection, the excess charge density distribution of planar  $Sc_2C$  and MNT-14 was calculated (Figure 4). Even upon a small amount of charge injection (0.01 e/atom), both excess holes and electrons

appear in the planar  $Sc_2C$  and MNT-14 (Figure S5), indicating that the intrinsic charge density distribution is perturbed.<sup>13,16,55</sup> For charge-injected planar  $Sc_2C$ , the excess charge density distributions are plotted in Figure 4a–d, showing that excess hole accumulates around Sc atoms both in the upper and lower atomic layers. Besides, the concentration of the excess hole around Sc atoms increases with increasing charge injection. Notably, compared with

![](_page_5_Figure_3.jpeg)

**Figure 6.** (a) Logarithmic scale for the relative  $C_5H_{12}$  transport rates across an electromechanically actuated MNT-6. Side and top views of the charge density difference of one  $C_5H_{12}$  through (b) pristine and (c,d) electromechanically actuated MNT-6 at the TS with an isosurface value of 0.0015 e/Bohr<sup>3</sup>. Herein, charge density difference of a  $C_5H_{12}$  through actuated MNT-6 with the radial actuation strains of (c) 8.3 and (d) 10.1% is plotted. Color coding consists of yellow for charge gain and green for charge loss.

excess charge density distribution of charge-injected planar Sc<sub>2</sub>C, the significant difference of charge-injected MNT-14 is that most of the excess hole accumulates in the outer atomic layer (Figure 4e,f). This significant difference between the inner and outer atomic layers of MNTs is supported by the above Bader charge analysis, showing that the Sc atom in the outer atomic layer loses more electrons than that in the inner atomic layer. Due to most of the excess hole distributed atop the outer atomic layer, the repulsive Coulomb interactions caused by the excess hole-hole pairs are mainly reflected on the outer atomic layer of the MNTs, resulting in radial actuation strain. Meanwhile, since the chemical binding connections exist between the inner and outer atomic layers, the change of interatomic parameters in the outer atomic layer would cause the change in the interatomic parameters in the inner atomic layer. From Figure 3b,c, the interatomic parameters with significant change are  $B_3$  and  $\theta_2$  that belong to the outer and inner atomic layers, respectively. In summary, on the one hand, the excess hole accumulate between Sc atoms of the planar Sc<sub>2</sub>C and MNTs (Figure 4) can result in repulsive Coulomb interaction, which largely explain the actuation strain. On the other hand, the depletion of electron (hole injection) can soften planar Sc<sub>2</sub>C and MNTs (see Structural Integrity of Planar Sc<sub>2</sub>C and MNTs under Electromechanical Loads for details). Therefore, the electromechanical actuation performance of planar Sc<sub>2</sub>C and MNTs is attributed to the Coulomb interaction of excess charge and softening of structures.

**Potential Applications of MNT Actuators.** At present, the existing nanochannels meet challenges in terms of stimulus complexity (e.g., solutions and ions) and response uncontrollability (e.g., low durability and response rate).<sup>36</sup> Considering the high electromechanical actuation performance, we propose potential uses of MNTs as tunable nanochannels and demonstrate this application by passing a molecule (neopentane,  $C_5H_{12}$ ) through MNT-6 with various actuated diameters. The diameter of pristine MNT-6 is 0.9 nm, and the kinetic diameter of the  $C_5H_{12}$  molecule is 0.6 nm.<sup>56</sup> The atomic configuration of MNT-6 with  $C_5H_{12}$  placed on its axial line is depicted in Figure 5a. For the calculation of  $C_5H_{12}$  passing through an electromechanically actuated MNT-6, a vacuum layer of 30 Å was used. The energy barrier ( $\Delta E$ ) for

 $C_5H_{12}$  passing through pristine and electromechanically actuated MNT-6 was calculated along the axial direction (Figure 5b), which is defined by<sup>57</sup>

$$\Delta E = E_{\rm TS} - E_{\rm SS} \tag{2}$$

where  $E_{TS}$  and  $E_{SS}$  are the total energies of the transition state (TS) and stable state (SS) of  $C_5H_{12}$  across electromechanically actuated MNT-6, respectively. The atomic configurations at the initial, transition, and final states are illustrated in Figure 5c. Before charge injection, the energy barrier is determined as 1.48 eV, indicating that  $C_5H_{12}$  cannot pass through pristine MNT-6 at a moderate temperature and pressure.<sup>58</sup> Afterward, the energy barriers of  $C_5H_{12}$  passing through an actuated MNT-6 with the equivalent radial actuation strains of 8.3% and 10.1% (corresponding to charge injections of 0.10 and 0.11 e/ atom, respectively, as shown in Figure S4a) are determined as 0.55 and 0.40 eV (Figure 5b), respectively. Compared with that (1.48 eV) passing through pristine MNT-6, these much lower energy barriers (0.40–0.55 eV) suggest that the  $C_5H_{12}$ molecule can easily pass through an actuated MNT-6 at a moderate temperature and pressure.<sup>52</sup>

Furthermore, we quantify the transport rates of a  $C_5H_{12}$  molecule passing through an electromechanically actuated MNT-6 by using the Arrhenius equation<sup>59</sup>

$$R = A e^{-\Delta E/k_{\rm B}T} \tag{3}$$

where *R*, *A*,  $k_{\rm B}$ , and *T* are the transport rate, prefactor, Boltzmann constant, and absolute temperature, respectively. The prefactor is identical for one molecule.<sup>60,61</sup> Based on eq 3, the relative transport rate of a C<sub>5</sub>H<sub>12</sub> through an electromechanically actuated MNT-6 compared with that through a pristine MNT-6 is derived as

$$P_{\text{actuated/pristine}} = \frac{Ae^{-\Delta E/k_{\text{B}}T}}{Ae^{-\Delta E_0/k_{\text{B}}T}} = e^{(\Delta E_0 - \Delta E)/k_{\text{B}}T}$$
(4)

where  $\Delta E_0$  and  $\Delta E$  are the energy barriers of  $C_5H_{12}$  passing through a pristine and an actuated MNT-6, respectively. Accordingly, the relative transport rates as functions of temperature were calculated as shown in Figure 6a, indicating the tunability of transport rates across multiscales. For example, the transport rate of  $C_5H_{12}$  passing through MNT-6 upon charge injection of 0.11 e/atom is 18 orders of

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magnitude higher than that passing through a pristine MNT-6 at 300 K. Hence, the tunability of the sieving diameters of MNTs is promising for tunable mass transport.

$$\Delta \rho = \rho_{\text{tot}} - \rho_{\text{MNT-6}} - \rho_{\text{C}_{\varsigma}\text{H}_{12}} \tag{5}$$

where  $ho_{
m tot}$   $ho_{
m MNT-6}$  and  $ho_{
m C5H12}$  are the charge densities of MNT-6 with one C<sub>5</sub>H<sub>12</sub>, MNT-6, and C<sub>5</sub>H<sub>12</sub>, respectively. The charge density difference is plotted in Figure 6b-d. Before charge injection, there is considerable charge overlap between  $C_5H_{12}$  and pristine MNT-6 (Figure 6b), indicating that  $C_5H_{12}$ is strongly pinned on the inner atomic layer of pristine MNT-6. This observation is consistent with the Bader charge analysis, which reveals that the total charge transfer between C<sub>5</sub>H<sub>12</sub> and pristine MNT-6 is 0.827 electrons. As shown in Figure 6c,d, the interaction of C5H12 with actuated MNT-6 is reduced, which is caused by the actuated diameter. The Bader charge analysis demonstrates that the charge transfer between a C<sub>5</sub>H<sub>12</sub> molecule and an electromechanically actuated MNT-6 decreases as the actuated diameter increases. The calculated charge transfer between  $C_5H_{12}$  and actuated MNT-6 with the radial actuation strains of 8.3% and 10.1% is 0.615 and 0.575 electrons, respectively. These results suggest that the actuated diameter of MNTs can effectively reduce the charge transfer between C5H12 and MNTs at the TS and hence eventually reduce the energy barrier.

### CONCLUSIONS

In summary, this work computationally demonstrate that MNTs exhibit high electromechanical actuation performance while maintaining sufficient structural integrity under a certain amount of charge injection. The maximum radial actuation strain of MNTs is as high as 26.8%. The underlying mechanism is elucidated by analysis through atomic- and electronic-scales. Finally, we explore the potential use of electromechanically actuated MNTs as tunable nanochannels by demonstrating the passage of a molecule ( $C_5H_{12}$ ) through an MNT with various actuated dimeters, indicating the tunability of transport rates across multiscales at a wide range of temperatures.

### ASSOCIATED CONTENT

#### **5** Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acs.jpcc.1c07453.

Illustrations of MNT-6 and MNT-10 structures and convergence test for the selected energy cutoff, temperature and system energy during AIMD simulations, calculations for the bending stiffness of planar  $Sc_2C$ , mechanical tests for MNTs and planar  $Sc_2C$  under the combined electromechanical loads, electromechanical actuation strain of MNT-6 and MNT-10 and their corresponding change of interatomic parameters, and excess charge density distribution of planar  $Sc_2C$  and MNT-14 upon 0.01 e/atom injection (PDF)

AIMD simulations of MNT-14 at 298 K for 10 ps (MP4)

MNT-14 upon charge injection (MP4)

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# AUTHOR INFORMATION

#### Corresponding Authors

- Ze Liu Department of Engineering Mechanics, School of Civil Engineering, Wuhan University, Wuhan, Hubei 430072, China; orcid.org/0000-0002-9906-5351; Email: ze.liu@ whu.edu.cn
- Enlai Gao Department of Engineering Mechanics, School of Civil Engineering, Wuhan University, Wuhan, Hubei 430072, China; orcid.org/0000-0003-1960-0260; Email: enlaigao@whu.edu.cn

#### Authors

- Bozhao Wu Department of Engineering Mechanics, School of Civil Engineering, Wuhan University, Wuhan, Hubei 430072, China
- Yuanpeng Yao Department of Engineering Mechanics, School of Civil Engineering, Wuhan University, Wuhan, Hubei 430072, China
- Ke Zhou State Key Laboratory for Strength and Vibration of Mechanical Structures, School of Aerospace Engineering, Xi'an Jiaotong University, Xi'an 710049, China;
   orcid.org/0000-0003-2239-4381

Complete contact information is available at: https://pubs.acs.org/10.1021/acs.jpcc.1c07453

#### **Author Contributions**

<sup>§</sup>B.W. and Y.Y. contribute equally.

# Notes

The authors declare no competing financial interest.

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# Supporting Information

# **Electromechanically Actuated MXene Nanotubes for Tunable Mass Transport**

Bozhao Wu<sup>1#</sup>, Yuanpeng Yao<sup>1#</sup>, Ke Zhou<sup>2</sup>, Ze Liu<sup>1\*</sup>, and Enlai Gao<sup>1\*</sup>

<sup>1</sup>Department of Engineering Mechanics, School of Civil Engineering, Wuhan University, Wuhan, Hubei

430072, China.

<sup>2</sup>State Key Laboratory for Strength and Vibration of Mechanical Structures, School of Aerospace Engineering,

Xi'an Jiaotong University, Xi'an 710049, China.

<sup>#</sup>These authors contribute equally.

\*Corresponding author. Email: ze.liu@whu.edu.cn; enlaigao@whu.edu.cn

![](_page_10_Figure_0.jpeg)

**Figure S1.** (a-b) Atomic configurations of (a) MNT-6 and (b) MNT-10. (c-d) Convergence tests for the energy cutoff. Evidently, the calculated actuation strains of planar Sc<sub>2</sub>C and MNT-6 using an energy cutoff of 400 eV are almost same to that using an energy cutoff of 520 eV, indicating that the energy cutoff of 400 eV provides a good balance between computational accuracy and effort.

![](_page_11_Figure_0.jpeg)

**Figure S2.** (a) Evolutions of temperature and system energy during AIMD simulations, which were performed at 298 K for 10 ps using Andersen thermostat to control the temperature (see Movie S1 for the animation). (b) Energy per nm<sup>2</sup> versus the radius (r) (herein, r is the radius of circular Sc<sub>2</sub>C): first principles calculations data (symbols) and continuum model (red solid lines, with a bending stiffness of 3.75 eV).

![](_page_12_Figure_0.jpeg)

**Figure S3.** Structural integrity under combined electromechanical loads. (a) Bilayer  $Sc_2C$  was used to determine the interlayer spacing ( $z_{eq}$ ). The unit cell is within the red dashed lines. (b) Tensile tests of planar  $Sc_2C$  upon charge injection of 0.20 e/atom. (c) Illustration of MNTs under the tension. (d) Tensile tests of MNTs upon charge injection.

![](_page_13_Figure_0.jpeg)

**Figure S4.** (a) Actuation performance of MNT-6 and MNT-10 upon charge injection. (b-e) Corresponding evolutions of the change of interatomic parameters of MNT-6 and MNT-10 as functions of charge injection. Changes of bond lengths ( $B_{1-4}$ ) and angles ( $\theta_{1-2}$ ) of (b-c) MNT-6 and (d-e) MNT-10 upon charge injection.

![](_page_14_Figure_0.jpeg)

**Figure S5.** (a) Excess charge density distributions of (a) planar  $Sc_2C$  and (b) MNT-14 upon 0.01 e/atom injection with the iso-surface value of 0.00015 and 0.00009 e/Bohr<sup>3</sup>, respectively. The yellow and blue colors represent excess electron and hole, respectively.

# **Supporting Information Movie 1:**

AIMD simulations of MNT-14 at 298 K for 10 ps.

# **Supporting Information Movie 2:**

MNT-14 upon charge injection.